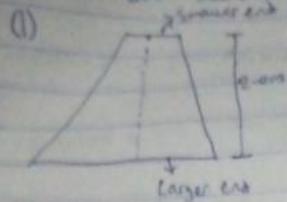


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Given

→ length of pipe $l = 2.0m$

velocity $v_1 = 5m/s$

velocity $v_2 = 2m/s$

Pressure head at the smaller end = 2.5m (i.e. $\frac{P_1}{\rho g} = 2.5$)

$$\text{Loss of head } h_L = \frac{0.35(v_1 - v_2)^2}{2g}$$

$$\therefore h_L = \frac{0.35(5 - 2)^2}{2 \times 9.81}$$

$$h_L = \frac{0.35(9)}{19.62} \Rightarrow \frac{3.15}{19.62} \Rightarrow 0.16m$$

Pressure head at lower end? (i.e. $\frac{P_2}{\rho g} = ?$)

Applying Bernoulli's equation, we have

$$\frac{P_1}{\rho} + \frac{v_1^2}{2g} + z_1 = \frac{P_2}{\rho} + \frac{v_2^2}{2g} + z_2 + h_L$$

Let $z_1 = 2.0m$
 $z_2 = 0m$

$$2.5 + \frac{5^2}{2 \times 9.81} + 2 = \frac{P_2}{\rho} + \frac{2^2}{2 \times 9.81} + 0 + 0.16$$

$$\Rightarrow 2.5 + 1.27 + 2 = \frac{P_2}{\rho} + 0.204 + 0.16$$

$$\frac{P_2}{\rho} = 5.27 - 0.364$$

$$\frac{P_2}{\rho} \Rightarrow \underline{\underline{5.41m \text{ of water}}}$$

(2)

→ Inlet diameter $D_1 = 20 \text{ cm} \rightarrow \text{m}$
 $\frac{20}{100} \Rightarrow 0.2 \text{ m}$

→ Area A_1 of inlet: $\frac{\pi D_1^2}{4} = \frac{\pi (0.2)^2}{4} \Rightarrow 0.0314 \text{ m}^2$

→ Throat diameter $D_2 = 10 \text{ cm} \rightarrow \text{m}$
 $\frac{10}{100} \Rightarrow 0.1 \text{ m}$

→ Area of Throat $A_2 = \frac{\pi D_2^2}{4} = \frac{\pi (0.1)^2}{4} \Rightarrow 0.00785 \text{ m}^2$

→ Pressure at inlet $P_1 = 17.658 \text{ N/cm}^2 \Rightarrow 17658 \text{ N/m}^2$

$\frac{P_1}{\rho} = \frac{17658}{9.81} \Rightarrow 18 \text{ m}$

→ Vacuum pressure at the throat.

$\frac{P_2}{\rho} = -30 \text{ cm} \rightarrow \text{m} \Rightarrow -0.3 \text{ m}$

$= -0.3 \text{ m of mercury} = -0.3 \times 13.6 \Rightarrow -4.08 \text{ m of water}$

→ Coefficient of discharge $C_d = 0.98$

∴ Differential head, $h = \frac{P_1 - P_2}{\rho} = 18 - (-4.08) \Rightarrow 22.08 \text{ m}$

Rate of flow, Q (Discharge of water through venturimeter)

$$Q = C_d \times \frac{A_1 A_2}{\sqrt{A_1^2 - A_2^2}} \times \sqrt{2gh}$$

$$Q = 0.98 \times \frac{0.0314 \times 0.00785}{\sqrt{(0.0314)^2 - (0.00785)^2}} \times \sqrt{2 \times 9.81 \times 22.08}$$

$Q = 0.165 \text{ m}^3/\text{s}$

③

→ Diameter of the pipe $D_1 = \frac{30 \text{ cm} \rightarrow \text{m}}{100} \Rightarrow 0.3 \text{ m}$

→ Area of the pipe $A_1 = \frac{\pi D_1^2}{4} = \frac{\pi (0.3)^2}{4} \Rightarrow 0.0706 \text{ m}^2$

→ Diameter of the orifice $D_0 = \frac{15 \text{ cm} \rightarrow \text{m}}{100} \Rightarrow 0.15 \text{ m}$

→ Area of the orifice $A_0 = \frac{\pi D_0^2}{4} = \frac{\pi (0.15)^2}{4} \Rightarrow 0.0176 \text{ m}^2$

→ Coefficient of discharge $C_d = 0.64$

→ Specific gravity of oil $S_o = 0.9$

→ Reading of differential manometer, $y = 50 \text{ cm} \rightarrow \text{m}$
 $\frac{50}{100} = 0.5 \text{ m}$

∴ Differential head, $h = y \left[\frac{S_m}{S_o} - 1 \right]$

8m of
oil

and $S_m = S_p$ gravity of heavier liquid = 13.6 (for mercury)

$$= 0.5 \left[\frac{13.6}{0.9} - 1 \right]$$

∴ 7.056 m of oil

Discharge $Q = C_d \frac{A_0 A_1 \sqrt{2gh}}{\sqrt{A_1^2 - A_0^2}}$

$$Q = \frac{0.64 \times 0.0176 \times 0.0706 \times \sqrt{2 \times 9.81 \times 7.056}}{\sqrt{0.0706^2 - 0.0176^2}}$$

$Q = 0.136 \text{ m}^3/\text{s}$

(c) Answer

→ Reading of the manometer, $y = 180 \text{ mm} \rightarrow \text{m}$

$$\frac{180}{1000} \Rightarrow 0.18 \text{ m of mercury}$$

→ Sp. gravity of mercury, $S_{H_2O} \Rightarrow 13.6$

→ Sp. gravity of Sea water, $S_c \Rightarrow 1.025$

$$\rightarrow \text{Head } h = y \left(\frac{S_{H_2O}}{S_c} - 1 \right)$$

$$h = 0.18 \left(\frac{13.6}{1.025} - 1 \right) = 2.09$$

\Rightarrow Speed of the Submarine

$$V = \sqrt{2gh}$$

$$V = \sqrt{2 \times 9.81 \times 2.09}$$

$$V = \underline{\underline{6.40 \text{ m/s}}}$$

~~(c) Answer~~

5)

$$\text{Actual flow rate} = \frac{50 \text{ m}^3/\text{min}}{60} = \frac{5 \times 10^{-3} \text{ m}^3/\text{sec}}{60} = 8.33 \times 10^{-5} \text{ m}^3/\text{s}$$

$$\text{Change in pressure, } \Delta P = 15 \text{ bar} = 15 \times 10^5 \text{ N/m}^2$$

$$\text{Speed of rotation, } \omega = \frac{1700 \text{ rev/min}}{60} = 28.33 \text{ rev/sec}$$

$$\text{Normal displacement} = \frac{10 \text{ cm}^3/\text{rev}}{10^6} = 1 \times 10^{-5} \text{ m}^3/\text{rev}$$

$$\text{Torque input, } T = 15 \text{ Nm}$$

$$\text{Volumetric Efficiency} = \frac{\text{Actual flow rate}}{\text{Ideal flow rate}} \times 100\%$$

$$\text{Actual flow rate} = 8.33 \times 10^{-5} \text{ m}^3/\text{sec}$$

$$\text{Ideal flow rate} = \text{Speed of rotation} \times \text{Normal displacement} = 28.33 \times 10^{-5} = 2.833 \times 10^{-4}$$

$$\therefore \text{Volumetric Efficiency} = \frac{8.33 \times 10^{-5} \times 100\%}{2.833 \times 10^{-4}} = 29.40\%$$

$$\text{Shaft Power, } P = Q \times \Delta P = 8.33 \times 10^{-5} \times 15 \times 10^5 = 124.95 \text{ Watts}$$

$$\text{Shaft Power} = T \cdot \omega = 15 \text{ Nm} \times 28.33 \text{ rev/s} = 424.95 \text{ W}$$

$$\therefore \text{Shaft power} = 5 \times 178.07 \\ = 2671.11 \text{ watts}$$

$$\text{Overall Efficiency} = \frac{\text{fluid power}}{\text{Shaft power}} \times 100\% \\ = \frac{124.95}{2671.11} \times 100\% \\ = 4.678\%$$

\therefore The overall efficiency is 4.678%

