

Question 10-6

Previous K-Chinda
15/13/2021

Parameters

$$\begin{aligned} \rho_o &= 4000 \text{ bbl/d} \\ Q_{DR} &= 500 \text{ scf/bbl} \\ D &= 3 \text{ inches} \\ e &= 0.001 \\ T &= 150^\circ \text{F} = 610^\circ \text{R} \\ P &= 200 \text{ psia} \\ \sigma_c &= 20 \text{ dyn/cm} \end{aligned}$$

$$\begin{aligned} \gamma_o &= 32^\circ \text{API} \\ \gamma_g &= 0.71 \\ N_1 &= 207 \\ N_g &= 0.013 \text{ scf} \\ T_{PC} &= 395^\circ \text{R} \\ P_{PC} &= 667 \text{ psia} \end{aligned}$$

Derived parameters

$$z = f\left(\frac{610}{395}, \frac{200}{667}\right) = 0.97$$

$$A = \left(\frac{\pi}{4}\right) \left(\frac{3}{12}\right)^2 = 0.0491 \text{ ft}^2$$

$$\gamma_o = \frac{141.3}{32 \cdot 1.315} = 0.865$$

$$C_o = 0.865 \times 62.4 = 54 \text{ lbm/ft}^3$$

$$C_g = \frac{28.97 \gamma_g P}{2 R T} = \frac{28.97 \times 0.71 \times 200}{0.97 \times 10.73 \times 610}$$

$$= 0.648 \text{ lbm/ft}^3$$

$$I_g = Q_{DR} \times \frac{1}{\rho_o}$$

$$z_g = 500 \times 4000 = 2 \times 10^6 \text{ ft}^2/\text{d}$$

Beggs and Brill method

flow regime calculation

$$\frac{USI}{A} = \frac{Q_1}{A} = \frac{4000 \times 5.615}{8.6400 \times 0.0491} = 5.2944 \text{ ft/s}$$

$$u_{sg} = \frac{4}{\pi D} \lambda \varepsilon \times z \times \left(\frac{T}{T_{sc}} \right) \times \left(\frac{P_{sc}}{P} \right)$$

$$= \frac{4}{\pi (3/12)^2} \times \frac{2 \times 10^4}{86400} \times 0.97 \times \frac{610}{520} \times \frac{14.7}{200}$$

$$u_{sg} = 39.4395 \text{ ft/s}$$

$$U_m = u_{si} + u_{sg} = 39.4395 + 5.2944 = 44.7339$$

$$\pi_1 = \frac{5.2944}{44.7339} = 0.11835$$

$$NFR = \frac{U_m^2}{gD} = \frac{44.7339^2}{32.17 \times 3/12} = 248.918$$

$$L_1 = 316 \times (0.11835)^{0.502} = 165.876$$

$$L_2 = 0.0009252 \times (0.11835)^{-2.4684} = 0.1795$$

$$L_3 = 0.1 \times (0.11835)^{-1.4316} = 2.3151$$

$$L_4 = 0.5 \times (0.11835)^{-5.738} = 104,023.273$$

flow is distributive. Since $\lambda < 0.4$ and $NFR > L_1$

Hold-up calculation

$$y_1 = y_{L_4}$$

$$y_{L_4} = a \lambda L^b$$

NFR^c

$$y_{10} = \frac{1.065 \times (0.11835)^{0.5829}}{248.818^{0.0609}}$$

$$y_{10} = \frac{0.3073}{1.3993} = 0.21961$$

$$C_n = 54 \times 0.11835 + 0.648 \times 0.88165$$

$$C_m = 6.9622 \text{ lbm/ft}^3$$

$$\mu_m = 2 \times 0.11835 + 0.0131 \times 0.88165 \\ = 0.24825$$

$$\mu_{\text{res}} = \frac{C_m \mu_m}{\mu_n} = \frac{6.9622 + 244.7339 \times \frac{2}{12}}{6.72 \times 10^{-4} \times 0.24825}$$

$$\mu_{\text{res}} = \frac{934.3391}{2.002 \times 10^{-3}}$$

$$\mu_{\text{res}} = 466728.96 \\ = 4.7 \times 10^5$$

$$F_n = 0.006$$

Calculations for X , S , f_{bP}

$$X = \frac{F_n}{J_0} = \frac{0.11835}{0.21961} = 2.454$$

$$S_2 = \ln(X)$$

$$S_2 = -0.0528 + 3.182 \ln(X) - 0.8725 [\ln(X) + 0.01853] \ln(X)$$

$$S_2 = 0.89772$$

$$2.8042 - 0.7031 + 0.012$$

$$S = \frac{0.89772}{2.1131} = 0.4248$$

$$f_{bP} = f_{nB}$$

$$f_{bP} = 0.006 \times e^{0.4248}$$

$$= 9.1757 \times 10^{-3}$$

$$= 0.009176$$

Frictional Pressure Losses Calculation

$$\left(\frac{dP}{dz}\right)_F = \frac{2f_{bP} \rho \mu_m^2}{J_0 D}$$

$$\frac{dP}{dz} = \frac{2 \times 0.009176 \times 6.9622 \times 44.7339^2}{32.17 \times \frac{2}{12}}$$

$$\frac{dp}{dz} = 31.792 \text{ lbf/ft}^2$$

$$= 31.792 \frac{\text{lbf}}{\text{ft}^2} \times \frac{1 \text{ft}^2}{144 \text{in}^2}$$

$$= 0.221 \text{ PSI/ft}$$

Calculation of mass flow rate.

$$m_1 = \rho_1 v_1$$

$$v_1 = \frac{4000 \text{ bbl} \times 5.615 \text{ ft}^3}{d \times 86400 \text{ s}} = 0.26 \text{ ft}^3/\text{s}$$

$$m_1 = 0.26 \text{ ft}^3/\text{s} \times 54 \text{ lbm/ft}^3 = 14.038 \text{ lbm/s}$$

$$m_2 = \rho_2 v_2$$

$$v_2 = \frac{2 \times 10^6 \text{ ft}^3}{d} \times \frac{1 \text{ ft}}{86400 \text{ s}} = \frac{2}{3} \times \frac{1}{48}$$

$$= A \times v_2 = 6.0491 \times 39.4395 = 1.93$$

$$m_2 = 1.936 \times 0.64 \text{ L/s}$$

$$= 1.255 \text{ lbm/s}$$

$$m = m_1 + m_2 = 14.038 + 1.255$$

$$m = 15.293 \text{ lbm/s}$$

gas velocity (Mg)

$$M_s = 0.0131 \times 6.72 \times 10^{-4}$$

$$= 8.8 \times 10^{-6} \text{ lbm/ft-sec}$$

Calculations f

$$\left[\frac{0.057 \text{ (Mg)} \text{ (m)} \text{ (m)}}{M_s} \right]^{0.5}$$

$$0.057 \text{ to } (1.255 + 15.293)^{0.5}$$

$$\frac{8.8 \times 10^{-6} \text{ (3/12)}^{2.25}}{0.24971} = 6.42 \times 10^5$$

$$0.24971$$

$$9.8891 \times 10^{-7}$$

$$\left(\frac{m_1}{m} \right)^{0.1} = 0.02$$

$$f = 0.02$$

$$\left(\frac{14.038}{15.293} \right)^{0.1} = 0.0202$$

$$\left(\frac{dP}{dx}\right) = \frac{f \ln \mu v^2}{2.9cD}$$

$$= \frac{0.0202 \times 6.9622 \times 44 \times 7339^2}{2 \times 32.17 \times (3/12)}$$

$$= 17.4966 \text{ lbf/ft}^3$$

$$= 0.122831 \text{ lbf/ft}$$

Darcy correlation

$$\frac{dP}{dx} = \left(\frac{dP}{dx}\right) + \left(\frac{dP}{dx}\right) K_e$$

frictional pressure drop

$$\left(\frac{dP}{dx}\right) f = \frac{f \rho_k \mu v^2}{2.9cD}$$

$$\rho_k = \frac{\rho_1 \bar{v}_1^2}{\gamma_1} + \frac{\rho_2 \bar{v}_2^2}{\gamma_2}$$

Assumes $\bar{v}_1 = \bar{v}_2$

$$\rho_1 = \rho_2$$

$$N_{Re1} = N_{Re2}$$

$$\bar{v}_1 = \bar{v}_2 = 0.11835$$

$$\rho_k = \frac{54 \times 0.11835^2}{0.11835} + \frac{0.648 \times 0.88165^2}{0.88165}$$

$$\rho_k = 6.962 \text{ lbf/ft}^3$$

$$N_{Rek} = 4.7 \times 10^5 \left(\frac{6.962}{6.9622} \right)$$

$$= 4.7 \times 10^5$$

$$f_n = 0.0056 + 0.5 (N_{Rek})^{-0.32}$$

$$= 0.0056 + 0.5 (4.7 \times 10^5)^{-0.32}$$

$$= 0.013$$

$$f = \frac{1}{\dots}$$

$$\frac{1}{f_n} = 1.2817 + 0.4778 \ln \bar{v}_1 + 0.444 (\ln \bar{v}_1)^2 + 0.09 (\ln \bar{v}_1)^3 + 0.00843$$

$$\frac{f}{f_n} = 1 - \sqrt{-2.134'' \cdot 2.81 - 1.0201 + 2.0222 - 0.9136 + 0.1749}$$

$$\frac{f}{f_n} = 1 - (-1.3818)$$

$$\frac{f}{f_n} = 2.3818$$

$$f = f_n \times 2.3818$$

$$f = 0.013 \times 2.3818$$

$$f = 0.031$$

$$\left(\frac{dp}{dx}\right) f = \frac{f \rho_k V_p^2}{2.9CD}$$

$$= \frac{0.013 \times 6.962 \times 44.7339^2}{2 \times 32.17 \times 0.25}$$

$$= 11.26 \text{ lbf/ft}^2 = 0.078 \text{ PSI/ft}$$

Question 10-4

Bakers Correction

$$A = (\pi/4) (2/12)^2$$

$$A = 0.02182 \text{ ft}^2$$

$$= 28.97 \text{ } \rho P$$

ZRT

$$= 28.97 \times 0.71 \times 1000$$

$$0.85 \times 10.73 \times 580$$

$$= 3.89 \text{ lbfm/ft}^3$$

$$\gamma_0 = \frac{141.5}{32 + 131.5} = 0.865$$

$$32 + 131.5$$

$$\rho_0 = 0.865 \times 62.9 = 54 \text{ lbfm/ft}^3$$

$$= \frac{\rho_L}{A} = \frac{500 \times 5.615}{86400 \times 0.02182} = 1.4892 \text{ ft}$$

$$= \frac{4}{\pi D^2} \times \rho \times Z \times \left(\frac{T}{TSC}\right) \times \left(\frac{PSC}{P}\right)$$

$$= \frac{4}{\pi D^2} \times \rho \times Z \times \left(\frac{T}{TSC}\right) \times \left(\frac{PSC}{P}\right)$$

$$= \frac{4}{\pi D^2} \times \frac{Q}{2} \times \dots$$

$$= \frac{4}{\pi (0.75)^2} \times \frac{500000}{86400} \times 0.85 \times \frac{580}{520} \times \frac{14.7}{1000}$$

$$= 3.697 \text{ ft/s}$$

$$\lambda = \left[\left(\frac{0}{0.075} \right) \left(\frac{0}{62.4} \right) \right]^{1/2}$$

$$\lambda = \left[\left(\frac{3.89}{0.075} \right) \left(\frac{54}{62.4} \right) \right]^{1/2}$$

$$\lambda = 6.6996$$

$$\phi = \frac{73}{\sigma_c} \left[\mu_2 \left(\frac{e_2 \cdot 4}{e_1} \right)^2 \right]^{1/3}$$

$$= \frac{73}{20} \left[2 \left(\frac{62.4}{54} \right)^2 \right]^{1/3}$$

$$d = 5.064$$

$$G_1 = U_{SS} \times P_S$$

$$= 3.697 \times 3.89 \times 3600 = 5.1773 \times 10^4$$

$$G_L = U_{SL} \times P_L$$

$$= 1.4892 \times 54 \times 3600 = 2.895 \times 10^5$$

$$G_1 = \frac{5.1773 \times 10^4}{6.6996} = 7.728 \times 10^3$$

$$\lambda = \frac{2.895 \times 10^5 \times 6.6996 \times 5.064}{5.1773 \times 10^4} = 189.71$$

slur flow, (i.e. flow is a function of $\frac{G_1}{\lambda}$, G_1 is from Beringer mcp)

mandhauw

flow (USL, USG)

$$VSL = 1.4892 \text{ ft/s}$$

$$VSG = 3.697 \text{ ft/s}$$

flow mandhauw flow map

flow regime = slow flow

Bess and Brill

flow = $f(NFR, \tau_e)$

$$NFR = \frac{U_m^2}{gD}$$

$$U_m = U_{SG} + U_{SL}$$

$$U_m = 1.4892 + 3.697 = 5.1862 \text{ ft/s}$$

$$g = 32.17 \text{ ft/sec}^2$$

$$D = \left(\frac{2}{12}\right) \text{ ft}$$

$$NFR = \frac{5.1862^2}{32.17 + \frac{2}{12}} = 5.0165$$

$$\tau_e = \frac{U_{SL}}{U_{SL} + U_{SG}} = \frac{1.4592}{1.4592 + 3.697}$$

$$\tau_e = 0.287$$

flow regime = Intermittent