**SIMON BOLIYEH DION**

**CIVIL ENGINEERING**

**17/ENG03/051**

**CVE 310: ENGINEERING SURVEY II**

**QUESTION ONE**

1. The methods of levelling are:
* Height of Collimation system
* Rise and Fall system

**HEIGHT OF COLLIMATION SYSTEM**

|  |  |
| --- | --- |
|  ADVANTAGES |  DRAWBACKS |
| * This method is rapid.
 | * There is no check on the reduced level of the intermediate sight.
 |
| * This method involves fewer calculations.
 | * Errors in the intermediate reduced levels cannot be detected.
 |
| * This method is suitable for levelling where there are a number of intermediate sights (longitudinal levelling).
 | * This system is not suitable for levelling where there are no intermediate sights (fly levelling).
 |
| * Reduction of levels is easy.
 | * There are only two checks on the accuracy of RL calculation.
 |

**RISE AND FALL SYSTEM**

|  |  |
| --- | --- |
|  ADVANTAGES |  DRAWBACKS |
| * There are checks on the reduced level of the intermediate sight.
 | * This method is slow.
 |
| * The errors in the intermediate reduced levels can be detected.
 | * This method involves a lot of calculations.
 |
| * This system is suitable for levelling where there are intermediate sights (fly levelling)
 | * This method is not suitable for levelling where there are a number of intermediate sights (longitudinal levelling)
 |
| * There are three checks on the accuracy of RL calculation.
 | * Reduction of levels is harder.
 |

1b.) R.L = 110 + Matriculation number; 110 + 51 = 161

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| B.S | I.S | F.S | H OF C | R.L | DISTANCE |
| 0.771 |  |  | 161.771 | 161 | 10 |
| 0.802 |  | 1.52 | 161.053 | 160.257 | 20 |
|  | 2.311 |  |  | 158.742 | 30 |
| 3.580 |  | 1.990 | 162.643 | 159.063 | 40 |
|  | 1.220 |  |  | 161.423 | 50 |
|  | 3.675 |  |  | 158.968 | 60 |
| 2.408 |  | 4.020 | 161.031 | 158.623 | 70 |
|  | 0.339 |  |  | 160.692 | 80 |
| 0.780 |  | 0.157 | 161.654 | 160.874 | 90 |
|  | 1.535 |  |  | 160.119 | 100 |
|  | 1.955 |  |  | 159.699 | 110 |
|  | 2.430 |  |  | 159.224 | 120 |
|  | 2.985 |  |  | 158.669 | 130 |
| 1.155 |  | 3.480 | 159.329 | 158.174 | 140 |
|  | 1.960 |  |  | 157.369 | 150 |
|  | 2.365 |  |  | 156.964 | 160 |
| 0.935 |  | 3.640 | 156.624 | 155.689 | 170 |
|  | 1.045 |  |  | 155.579 | 180 |
|  | 1.630 |  |  | 154.994 | 190 |
|  |  | 2.545 |  | 154.079 | 200 |
| $Σ$=10.431 |  | $Σ$=17.352 |  |  |  |

Check=$ΣF.S-ΣB.S$=R.L at first point-R.L at last point

 =6.921=6.921

HC= RL + BS

HC(1) = 161+0.771=161.771

RL = HC-FS

RL(1)=161.771-1.52=160.251

HC(2)= 160.251+ 0.802=161.053

RL(2)= 161.053 – 2.311 =158.742

RL(3)=161.053-1.990=159.063

HC(3)=159.063+3.580=161.643

RL(4)=162.643-1.220=161.423

RL(5)=162.643-3.675=158.968

RL(6)=162.643-4.020=158.623

HC(4)=158.623+2.408=159.031

RL(7)= 156.031-0.339=160.692

RL(8)= 161.031-0.157=160.874

HC(5)=161.654+0.780=161.654

RL(9)= 161.654-1.535=160.119

RL(10)= 161.654-1.955=159.699

RL(11)= 161.654-2.430=159.224

RL(12)= 161.654-2.985=158.669

RL(13)= 161.654-3.480=158.174

HC(6)=159.329+1.155=159.329

RL(14)= 159.329-1.960=157.369

RL(15)= 159.329-2.365=156.964

RL(16)= 159.329-3.640=155.689

HC(7)=155.689+0.935=155.624

RL(17)= 156.624-1.045=155.579

RL(17)= 156.624-1.630=154.994

RL(17)= 156.624-2.545=154.079



**QUESTION TWO**

|  |  |  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| Chainage(m) | 0 | 30 | 60 | 90 | 120 | 150 | 180 | 210 | 240 | 270 |
| Offset length(m) | 0 | 2.65 | 3.80 | 3.75 | 4.65 | 3.60 | 5.00 | 5.80 | 6.10 | 5.85 |

1. **Using Mid-ordinate rule:**

A=$Σ$hd

h1= $\frac{0+2.65}{2}$=1.325m

h2= $\frac{2.65+3.80}{2}$=3.225m

h3= $\frac{3.80+3.75}{2}$=3.775m

h4= $\frac{3.75+4.65}{2}$=4.2m

h5= $\frac{4.65+3.60}{2}$=4.125m

h6= $\frac{3.60+5.00}{2}$=4.3m

h7= $\frac{5.00+5.80}{2}$=5.4m

h8= $\frac{5.80+6.00}{2}$=5.9m

h9= $\frac{6.00+5.85}{2}$=5.925m

$$Σh=1.325+3.225+3.775+4.2+4.125+4.3+5.4+5.9+5.925$$

$Σh=$38.175m

d=30m

A=$Σhd$

= $38.175×30$

A= $1145.25m^{2}$

1. **Using average ordinate rule:**

A=$\frac{ndΣO}{n+1}$

n=9

d=30

$$ΣO=0+2.65+3.80+3.75+4.65+3.60+5.00+5.80+6.10+5.85$$

$ΣO=$41.2m

A=$\frac{9×30×41.2}{9+1}$

A=$112.4m^{2}$

1. **Using trapezoidal rule:**

A=$d(\frac{0\_{1}+0\_{n }}{2}+0\_{2}+0\_{3}+0\_{4}............0\_{n-1})$

$$d=30$$

A=$30(\frac{0+5.85}{2}+2.65+3.80+3.75+4.65+3.60+5.00+5.80+6.10)$

A=$30(38.275)$

A=$1148.25m^{2}$

1. **Using Simpson's rule:**

$$A=\frac{d }{3 }\left[\left(0\_{1}+0\_{n}\right)+4\left(0\_{2}+0\_{4}+.........0\_{n-1}\right)+2\left(0\_{3}+0\_{5}........0\_{n-1}\right)\right]$$

$$d=30$$

Note: Last offset was removed because number of offsets were even

$$A=\frac{30}{3 }\left[\left(0+6.10\right)+4\left(2.65+3.75+3.60+5,80\right)+2\left(3.80+4.65+5.00\right)\right]$$

$$A=962m^{2}$$

Calculating for last offset using trapezoidal rule

A=$d(\frac{0\_{1}+0\_{n }}{2}+0\_{2}+0\_{3}+0\_{4}............0\_{n-1})$

$$A=30\left[\frac{6.40+5.85}{2}\right]$$

$$A=183.75m^{2}$$

Therefore $ΣA=962+183.75$

$$A=1145.75m^{2}$$

1. **CHARACTERISTICS OF CONTOURS**
2. Contour lines cross a watershed or ridge line at right angles. They form curves of U-shape round it with the concave side of the curve towards the higher ground.

 

1. Contour lines with V-shaped with convexity towards higher ground at right angles indicate valley.
2. Contour lines meeting at a point indicate a vertical cliff.



1. A series of closed contour lines on the map indicates a depression if the higher values are outside.



1. A series of closed contour lines on the map represents a hill, if the values are inside.

