

NAME SANNI ABDULRAHMAN

MAT NO. 17/ENG03/050

COURSE STRUCTURAL DESIGN (CVE 308)

- i) The design must be economical
- ii) To design for safety
- iii) The deformation of the structure must not impose with the integrity of the structure

b) Limit state design considers the disadvantages of load factor design and any other failure that can cause the structure to be structure. Unlike elastic design is a method of analysis which the design of a structural member is based on a linear stress - strain relationship, assuming that the working stress are only a fraction of the elastic limit of the material.

## STAIR CASE DESIGN

$$\text{Slope Factor} = \frac{\sqrt{R^2 + T^2}}{T} = \frac{\sqrt{150^2 + 275^2}}{275}$$

$$= 1.14$$

### \* Load Analysis

- $\text{KLAIST} = R \times 24 \text{ kN/m}^2$

$$= 0.15 \times 24 = 3.6 \text{ kN/m}^2$$

- $\text{FINISHES} = 1.2 \text{ kN/m}^2$

- $\text{STEPS} = T \times \frac{1}{2} \times 24 \text{ kN/m}^2$

$$0.275 \times 0.5 \times 24 = 3.3 \text{ kN/m}^2$$

$$\Delta \cdot G \cdot K = (A + B) \times S_f + C$$

$$= (4.8 \times 1.14) + 3.3$$

$$= 8.77 \text{ kN/m}$$

$$\Delta \cdot L, F = 1.4 G_k + 1.6 Q_k$$

$$1.4 (8.77) + 1.6 (1.5)$$

$$14.63 \text{ kN/m}^2$$

$$S_{Pen} = T_{total} + 0.5(l_c + l_b) \\ (275 \times 12) + 0.5(225 + 225) = 3.525 \text{ m}$$

$$d = h_{cover} - \frac{1}{2} \phi \\ = 150 - 25 - 6 = 119 \text{ mm}$$

$$M = \frac{FL^2}{10} = \frac{14.68 \times 3.525^2}{10} = 18.24 \text{ kNm}$$

$$k = \frac{18.24 \times 10^6}{1600 \times 19^2 \times 25} = 0.052$$

$$I_{e1} = 0.5 + \sqrt{0.25 - 0.052/0.9} = 0.938$$

$$Z = I_{e1} d = 0.938 \times 119 = 111.622 \text{ mm}$$

$$A_s = \frac{18.24 \times 10^6}{0.95 \times 410 \times 111.622} = 419.53$$

$$A_{s,prov} = 452 \text{ mm}^2$$

Provide 4/12 @ 259 c/c ( $A_{s,prov} = 452 \text{ mm}^2$ )

Deflection check

$$f_s = \frac{2}{3} \times 1 \times \frac{419.53}{452} \times 250 = 154.69 \text{ N/mm}^2$$

$$M.F.S. = 0.55 + \frac{477 - 154.69}{120}$$

$$= 0.55 + \frac{18.24 \times 10^6}{1600 \times 119^2} = 1.78$$

$$d_{req} = \frac{3525}{1.78 \times 26} = 76.17 \text{ mm}$$

Since  $d_{req} < d$ , Deflection is OK

$$2a) P_1 = P_2 = P_3 = \frac{4300}{4000} = 1.075 < 2 = 2 \text{ way slab}$$

$$P_4 = P_5 = P_6 = \frac{4300}{4000} = 1.075 < 2 = 2 \text{ way slab}$$

$$P_7 = P_8 = P_9 = \frac{4500}{4000} = 1.125 < 2 = 2 \text{ way slab}$$

$$P_{10} = P_{11} = P_{12} = \frac{4000}{1500} = 2.66 > 2 = 1 \text{ way slab}$$

2b) Designing  $P_2$

$$l_y/l_x = 4300/4000 = 1.075 \leq 1.1$$

$$\text{Short span coefficient} = 0.054$$

$$\text{Long span coefficient} = 0.644$$

Assuming specifications

$$\text{Height of slab} = 0.175 + 24$$

$$\text{Partition} = 1.0$$

$$\text{Finishes} = 1.2$$

$$6.4 \text{ kN/m}^2$$

Assuming for factory

$$(1.4 \times 6.4) + (1.6 \times 5)$$

$$= 16.96 \approx 17 \text{ kw/m}^2$$

$$\text{Short span Coefficient} = \frac{0.044}{0.033}$$

$$\text{long span Coefficient} = \frac{0.032}{0.028}$$

Short span mid = P

$$M = B \times w \times l^2 \times c = 0.044 \times 17 \times 4^2 = 11.968$$

$$d = (h - \text{cover}) \times \frac{1}{2} = 144$$

$$k = \frac{M}{b d^2 l c} = \frac{11.968 \times 10^4}{1000 \times 144^2 \times 25} = 0.023$$

$$I_a = 0.5 + \sqrt{0.25 \times k / 0.0196} = 0.97 > 0.95$$

$$Z = I_a d = 0.95 \times 144 = 136.8$$

$$A_s = \frac{11.968 \times 10^4}{0.95 \times 40 \times 136.8} = 224.61$$

Provide 4, 2 @ 377mm

$$M = 82 w l^2 \Rightarrow 0.033 \times 17 \times 4^2 = 8.976$$

$$d = 144$$

$$h = \frac{8.976 \times 10^6}{1000 \times 144^2 \times 2.5} = 0.0173$$

$$I_a = 0.5 + \sqrt{0.25 - 14(0.9)} = 0.83$$

$$z = I_a d = 0.83 \times 144 = 119.52$$

$$A_s = \frac{8.976 \times 10^6}{0.95 \times 410 \times 119.52} = 192.81 \text{ mm}^2$$

$$0.95 \times 410 \times 119.52$$

Provide  $4 \phi_{12} @ 377 \text{ mm}$

Long Span = Mid

$$d(\text{short span}) = \text{Steel thickness} \times 12 + 12 = 132 \text{ mm}$$

$$M = 0.037 \times 17 \times 4^2 = 10.064$$

$$k = \frac{10.064 \times 10^6}{1000 \times 132^2 \times 2.5} = 0.0281$$

$$I_a = 0.5 + \sqrt{0.25 - 0.0281/0.9} = 0.97 > 0.95$$

$$z = 0.95 \times 132 = 125.4$$

$$A_s = \frac{10.064 \times 10^6}{0.95 \times 125.4 \times 410} = 206.04$$

$$0.95 \times 125.4 \times 410$$

Provide  $4 \phi_{12} @ 377 \text{ mm}$

Continuous

$$d = 132 \text{ mm}$$

$$M = 0.028 \times 17 \times 4^2 = 7.616$$

$$k = \frac{M}{bd^2 l_{cr}} = \frac{7.616 \times 10^6}{1000 \times 132^2 \times 25} = 0.017$$

$$I_{cr} = 0.5 + \sqrt{0.25 - 0.017/0.9} = 0.98 > 0.95$$

$$Z = 0.95 \times 132 = 125.4$$

$$A_s = \frac{7.616 \times 10^6}{0.95 \times 410 \times 125.4} = 155.93$$

Provide  $\phi 12 @ 377 \text{ mm}$

Deflection check

$$f_s = 2/3 + 250 \times 1 \times \frac{224.61}{377} = 99.3$$

$$m_{IR} = 0.55 + \frac{422 - 99.3}{120 \left( 0.9 + \frac{11.963 \times 10^6}{1000 \times 1442} \right)} = 2.68 > 2$$

$$d_{req} = \frac{4 \times 1000}{2 \times 26} = 76.92 = 77 \text{ mm}$$

d<sub>req</sub> is ok