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17/ENG03/040

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CIVIL ENGINEERING CUE308

STRUCTURAL DESIGN ASSIGNMENT

- To design for safety
- The design must be economical
- The deformation of the structure must not impose with the intensity of the structure

1b) Limit Slab design considers the disadvantages of Load Factor design and any other failure that can cause the structure to be structurally unfit while elastic design is a method of analysis which the design of a structural member is based on the linear stress-strain relationship assuming that the working stress are only a fraction of the elastic limit of the materials

STAIRCASE DESIGN

$$\text{Slope Factor} = \frac{\sqrt{R^2 + T^2}}{T} = \frac{\sqrt{150^2 + 275^2}}{275} = 1.14$$

*Load Analysis

$$A. \text{Waist} = R \times 24 \text{ kN/m}^2 = 0.15 \times 24 = 3.6 \text{ kN/m}^2$$

$$B. \text{Finishes} = 1.2 \text{ kN/m}^2$$

$$C. \text{STEPS} = T \times \frac{1}{2} \times 24 \text{ kN/m}^2 = 0.275 \times 0.5 \times 24 = 3.3 \text{ kN/m}^2$$

$$D. G.K = ((A+B) \times S.F) + C = (4.8 \times 1.14) + 3.3 = 8.77 \text{ kN/m}$$

$$D.L, F = 1.4 G.K + 1.6 Q.K = 1.4(8.77) + 1.6(1.5) = 14.68 \text{ kN/m}^2$$

$$\text{Span} = l_{\text{Total}} + 0.5(l_a + l_b) = (275 \times 12) + 0.5(225 + 225) = 3.525$$

$$d = h - \text{Cover} - \frac{1}{2} \phi$$

$$= 150 - 25 - 6 = 119 \text{ mm}$$

$$M = \frac{Fl^2}{10} = \frac{14.68 \times 3.525^2}{10} = 18.24 \text{ kNm}$$

$$K = \frac{M}{bd^2 f_{cu}} = \frac{18.24 \times 10^6}{1000 \times 119^2 \times 25} = 0.052$$

$$I_a = 0.5 + \sqrt{0.25 - \frac{K}{0.9}} = 0.5 + \sqrt{0.25 - \frac{0.052}{0.9}} = 0.938$$

$$Z = I_a d = 0.938 \times 119 = 111.622 \text{ mm}$$

$$A_s = \frac{M}{0.95 f_y Z} = \frac{18.24 \times 10^6}{0.95 \times 410 \times 111.622} = 419.53$$

$$A_{s \text{ prov}} = 452 \text{ mm}^2$$

Provide $Y12 @ 259 \text{ c/c}$ (A_{s prov} = 452 mm²)

Deflection Check

$$f_s = \frac{2}{3} \times 1 \times \frac{A_{\text{req}}}{A_{\text{prov}}} \times f_{yv} = \frac{2}{3} \times 1 \times \frac{419.53}{452} \times 250$$

$$f_s = \frac{2}{3} \times 1 \times \frac{419.53}{452} \times 250$$

$$M.F = 0.56 + \frac{477 - 154.69}{120(0.9 + \frac{18.24 \times 10^6}{1000 \times 119^2})} \times 20 \times 250 = 1.78 \times T = 2972$$

$$d_{\text{req}} = \frac{\text{Span}}{nf \times edv} = \frac{3.525}{1.78 \times 26} = 76.17 \text{ mm}$$

Since $d_{\text{req}} < d$, Deflection is OK

$$2a) P_1 = P_2 = P_3 = \frac{4300}{4000} = 1.075 < 2 = \text{2way slab}$$

$$P_2 = P_8 = P_9 = \frac{4500}{4000} = 1.125 < 2 = \text{2way slab}$$

$$P_4 = P_5 = P_6 = \frac{4300}{4000} = 1.075 < 2 = \text{2way slab}$$

$$P_{10} = P_{11} = P_{12} = \frac{4000}{1500} = 2.666 > 2 = \text{1way slab}$$

Designing P_2

$$\frac{l_y}{l_x} = \frac{4300}{4000} = 1.075$$

Short span coefficient = -

$$\text{Longspan coefficient} = \frac{0.058}{0.044}$$

Specification of Slab thickness = 175mm

$$f_{cu} = 25 \text{ N/mm}^2$$

$$f_y = 410 \text{ N/mm}^2$$

$$DL = 1.4 GK + 1.6 QK$$

$$G-K = \text{weight of slab} = 0.175 \times 24$$

$$\text{Partitions} = 1.0$$

$$\text{Finishes} = 1.2$$

$$= 16.96 \text{ kN/m}^2$$

Assuming for factory

$$D-L = (1.4 \times 6.4) + (1.6 \times 5) = 16.96 = 17 \text{ kN/m}^2$$

$$\text{Shortspan Coefficient} = 0.044$$

$$0.033$$

$$\text{Long span Coefficient} = 0.032$$

$$0.028$$

$$\text{Short span } m \cdot d = P$$

$$M = B \times W L^2 \alpha = 0.044 \times 17 \times 4^2 = 11.968$$

$$d = h - \text{Cover} - \frac{1}{2} \phi = 144$$

$$k = \frac{M}{bd^2 f_{cu}} = \frac{11.968 \times 10^6}{1000 \times 144^2 \times 25} = 0.023$$

$$I_a = 0.5 + \sqrt{0.25 - \frac{k}{0.9}} = 0.97 > 0.95 = 0.95$$

$$Z = I_a \cdot d = 0.95 \times 144 = 136.8$$

$$A_s = \frac{M}{0.95 f_y z} = \frac{11.968 \times 10^6}{0.95 \times 410 \times 136.8} = 224.61$$

Provide $Y_{12} @ 377\text{mm}$

Continuous

$$M = B \times W L^2 \alpha = 0.033 \times 17 \times 4^2 = 8.976$$

$$d = 144$$

$$k = \frac{M}{bd^2 f_{cu}} = \frac{8.976 \times 10^6}{1000 \times 144^2 \times 25} = 0.0173$$

$$I_a = 0.5 + \sqrt{0.25 - \frac{k}{0.9}} = 0.5 + \sqrt{0.25 - \frac{0.0173}{0.9}} = 0.83$$

$$Z = I_a \cdot d = 0.83 \times 144 = 119.52$$

$$A_s = \frac{M}{0.95 f_y z} = \frac{8.976 \times 10^6}{0.95 \times 410 \times 119.52} = 192.81\text{mm}^2$$

Provide $Y_{12} @ 377\text{mm}$

Long Span
Mid

$$d = d(\text{Shortspan}) \text{ Steel thickness} = 144 - 12 = 132 \text{ mm}$$

$$M = B \times w l^2 \times c = 0.037 \times 17 \times 4^2 = 10.064$$

$$K = \frac{M}{bd^2 f_{cu}} = \frac{10.064 \times 10^6}{1000 \times 132^2 \times 25} = 0.0231$$

$$I_a = 0.5 + \sqrt{0.25 - \frac{K}{0.9}} = 0.97 > 0.95 = 0.95$$

$$Z = I_a \cdot d = 0.95 \times 132 = 125.4$$

$$A_s = \frac{M}{0.95 f_y z} = \frac{10.064 \times 10^6}{0.95 \times 125.4 \times 410} = 206.04$$

provide y_{12} at 377mm

Long Span Continuous

$$d = 132 \text{ mm}$$

$$M = B \times w l^2 \times c = 0.028 \times 17 \times 4^2 = 7.616$$

$$K = \frac{M}{bd^2 f_{cu}} = \frac{7.616 \times 10^6}{1000 \times 132^2 \times 25} = 0.017$$

$$I_a = 0.5 + \sqrt{0.25 - \frac{K}{0.9}} = 0.98 > 0.95 = 0.95$$

$$Z = I_a \cdot d = 125.4$$

$$A_s = \frac{M}{0.95 f_y z} = \frac{7.616 \times 10^6}{0.95 \times 410 \times 125.4} = 155.93$$

provide y_{12} @ 377mm

Deflection check

$$f_s = \frac{2}{3} P_y r B \frac{A_{req}}{A_s \text{ approved}}$$

$$F_s = \frac{2}{5} \times 250 \times 1$$

$$= \frac{224.61}{377} = 99.3$$

$$M.R = 0.55 + \frac{477 - 99.3}{120(0.9) + \frac{11.968 \times 10^6}{1000 \times 144^2}} = 2.68 > 2$$

$$d_{req} = \frac{4 \times 1000}{2 \times 26} = 76.92 = \text{OK}$$