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1b) To design for safety

b) The design must be economical

c) The deformation of the structure must not impose with the integrity of the structure

1b) Limit state design considers the two advantages of load factor design and any other failure that can cause the structure to be structurally unfit while elastic design is a method of analysis in which the design of a structural member is based on a linear stress-strain relationship assuming that the working stress are only a fraction of the ^{elastic} limit of the material

STAIR CASE DESIGN

$$\text{Slope factor } \frac{\sqrt{R^2 + I^2}}{R} = \frac{\sqrt{150^2 + 275^2}}{150} = 1.14$$

$$A = 0.15 \quad T = 275$$

* Load Analysis

$$A \text{ WAIST} = R \times 24 \text{ kN/m}^2 \\ = 0.15 \times 24 = 3.6 \text{ kN/m}^2$$

$$* B \text{ Finish } 1.2 \text{ kN/m}^2$$

$$C \text{ steps} = T \times 1/2 = 24 \text{ kN/m}^2$$

$$= 0.275 \times 0.5 \times 24 = 3.3 \text{ kN/m}^2$$

$$D. G. C = (C(A+B) + SF) + C$$

$$= (4.8 \times 1.14) + 3.3$$

$$= 8.77 \text{ kN/m}$$

$$D.G.F = 1.4 G.C + 1.6 Q.C$$

$$= 1.4 (8.77) + 1.6 (1.5)$$

$$= 14.14 \text{ kN/m}^2$$

$$\text{Span} = \text{Total} + \text{Case (at } l_b) = 27.5(12) + 0.5(225/225)$$

$$= 3.527 \text{ m}$$

$$d = h - \text{cover} - \frac{1}{2} \phi$$

$$= 150 - 25 - 6 = 119 \text{ mm}$$

$$M = f_t^2 = 18.24 \times 10^6 = 18.24 \text{ MNm}$$

$$k = \frac{M}{I} = \frac{18.24 \times 10^6}{110^4 \times 25} = 0.012$$

$$I_a = 0.57 \sqrt{0.25 \times 119} = 0.57 \sqrt{29.75} = 0.938$$

$$Z = I_a d = 0.938 \times 119 = 111.622 \text{ m}$$

$$A_s = M = \frac{18.24 \times 10^6}{0.938 \times 410} = 419.53$$

$$A_s \text{ per} = 452 \text{ mm}$$

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Provide 9/12 @ 259 C/C (A_{per} = 452 mm)

Deflection check

$$f_s = \frac{2}{3} \times \frac{1}{6} \times \frac{M_{max}}{A_s \text{ per} \times f_y \times v}$$

$$f_s = \frac{2}{3} \times \frac{1}{6} \times \frac{419.53}{452} \times 250 = 154.69 \text{ mm}^2$$

$$M_{EF} = 0.56 + \frac{4.77 - 154.69}{120(0.9 + 18.24 \times 10^6)} = 1.78$$

$$d_{req} = \frac{\text{span}}{atxedr} = \frac{3.525}{1.78 \times 120} = 76.17 \text{ mm}$$

Since $d_{req} < d$, deflection is ok

$$2a) P_1 = P_2 = P_3 = \frac{4300}{4000} = 1.075 < 2 = 2 \text{ way slab}$$

$$P_2 - P_4 = P_5 = \frac{4000}{4000} = 1.125 < 2 = 2 \text{ way slab}$$

$$P_4 = P_5 = P_6 = \frac{4300}{4000} > 1.075 < 2 = 2 \text{ way slab}$$

$$P_{10} = P_{11} = P_{12} = \frac{4000}{1500} = 2.66 > 2 = 1 \text{ way slab}$$

Designing for P_2

$$l_y = 4300 \quad \text{---} \quad 1.05 = \approx 1.1$$

$$l_x = 4000$$

Short span coefficient

$$0.071$$

Long span coefficient

$$0.044$$

Assuming specification of slab thickness

$$= 175 \text{ mm}$$

$$f_{cu} = 25 \text{ N/mm}^2$$

$$f_y = 460 \text{ N/mm}^2$$

$$DL = 1.4 G_k + 1.6 Q_k$$

$$G_k = \text{weight of slab} = 0.175 \times 24$$

$$\text{particular} = 1.0$$

$$\text{Finish} = 1.2$$

$$6.4 \text{ kN/m}^2$$

Assuming for safety

$$DL = (1.4 \times 6.4) + (1.6 \times 5)$$

$$= 16.96 \approx 17 \text{ kN/m}^2$$

Short span coefficient

$$0.033$$

Long span coefficient

$$0.028$$

Short span $m_1 = P$

$$m = \frac{w l^2}{8} = 0.071 \times 4300^2 \times 17$$
$$= 11.968$$

$$I = h^3 \times 12 = \frac{1}{2} \times 12 \times h^3$$

$$h = \sqrt[3]{\frac{m}{12 \times f_{cu}}} = \sqrt[3]{\frac{11.968 \times 10^6}{1000 \times 12 \times 25}} = 0.23$$

$$1000 \times 12 \times 25$$

$$e = \frac{P}{A} = 0.5 + \sqrt{0.25 - \frac{e}{d}} = 0.977 \times 0.95 = 0.928$$

$$d = \frac{P}{A} = 0.95 \times 144 = 136.8$$

$$AS = \frac{m}{0.95 \times 12} = \frac{11.968 \times 10^6}{0.95 \times 12 \times 136.8}$$

$$224.61$$

Provide 412 @ 377mm

Continuous

$$M = b x u x l^2 = 0.033 \times 117 \times u^2 = 3.77u$$

$$l = 12u$$

$$u = \frac{M}{b^2 d f_{cu}} = \frac{3.776 \times 10^6}{1000 \times 125^2 \times 12.5} = 0.0173$$

$$p_a = 0.5 + \sqrt{0.25 - \frac{u}{0.9}} = 0.5 + \sqrt{0.25 - \frac{0.0173}{0.9}} = 0.33$$

$$z = p_a \cdot l = 0.33 \times 12u = 119.52$$

$$A_s = \frac{M}{0.95 p_y z} = \frac{3.776 \times 10^6}{0.95 \times 410 \times 119.52} = 192.11 \text{ mm}^2$$

Provide 412 @ 377mm

Long span

msd

$l = d$ (short span) = steel thickness

$$= 1244 - 12 = 1232 \text{ mm}$$

$$M = b x u x l^2 = 0.037 \times 117 \times u^2 = 10.06u$$

$$u = \frac{M}{b^2 d f_{cu}} = \frac{10.06 \times 10^6}{1000 \times 32^2 \times 12.5} = 0.0231$$

$$p_a = 0.5 + \sqrt{0.25 - \frac{u}{0.9}} = 0.97 \quad 0.95 = 0.95$$

$$z = p_a \cdot d = 0.95 \times 1232 = 1170.4$$

$$A_s = \frac{M}{p_a \cdot f_y \cdot z} = \frac{10.06 \times 10^6}{0.95 \times 410 \times 1170.4} = 2.06$$

$$= 2060 \text{ mm}^2$$

Provide 412 at 317mm

Less span continues

$$l = 132 \text{ mm}$$

$$M = b x u x l^2 = 0.025 \times 12 \times u^2 = 2.06u$$

$$lc = \frac{M}{b d^2 f_{cu}} = \frac{2.616 \times 10^6}{1000 \times 125^2 \times 25} = 0.017$$

$$\rho_{cc} = 0.5 + \sqrt{0.4 + \frac{lc}{0.9}} = 0.98 > 0.95$$

$$= 0.95$$

$$Z = \rho_s \cdot d = 125.4$$

$$A_s = \frac{M}{\rho_s f_{yk} Z} = \frac{2.616 \times 10^6}{0.95 \times 1100 \times 125.4} = 153.93$$

provide y12 @ 377mm

detention length

$$f_s = 2/3 \rho_s B \frac{\text{Area}}{\text{Aspacer}}$$

$$f_s = 2/3 \times 250 \times 1 \times \frac{224.01}{377} = 99.3$$

$$m: f_c = \frac{0.55 + 4.22 - 99.3}{110(0.9 + \frac{11.988 \times 10^6}{1000 \times 125^2})} = 2.6873$$

$$I_{req} = \frac{M \times 1000}{2 \times 10} = 79.62 \times 10^6$$