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Mechanical Engineering

4) Compute the dimensions of a flanged cast iron pipe 200mm in diameter to carry a pressure of 0.7 N/mm^2

Solution.

$$D = 200 \text{ mm}$$

$$P = 0.7 \text{ N/mm}^2$$

$$\sigma_t = 14 \text{ N/mm}^2 \text{ from table 8.1}$$

$$C = 9 \text{ mm from table 8.2}$$

$$\text{thickness } t = \frac{PD}{2\sigma_t} + C$$

$$t = \frac{0.7 \times 200 + 9}{2 \times 14}$$

$$t = 14 \text{ mm}$$

Other dimensions of a flanged joint for a cast iron pipe are:

* Nominal diameter of bolts

$$d = 0.75k + 10$$

$$= 0.75 \times 14 + 10$$

$$= 20.5 \text{ mm} \approx 21 \text{ mm}$$

* Number of bolts = $0.0275D + 1.6$

$$n = 0.0275 \times 200 + 1.6 = 4.1 \approx 8 \text{ mm}$$

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• Thickness of the flange

$$t_f = 1.5t + 3$$

$$= 1.5 \times 14 + 3 = 24 \text{ mm}$$

~~• Outside diameter of the bolts~~

~~$$D_o = D + 2t + 2B$$~~

~~$$= 200 + 2(14) + 2(50) = 328 \text{ mm}$$~~

~~• Width of the flange =~~

~~$$B$$~~

• Width of the flange

$$B = 2.3 \times d$$

$$2.3 \times 21 = 48.3 \approx 50 \text{ mm}$$

• Outside diameter of the bolts

$$D_o = D + 2t + 2B$$

$$200 + 2(14) + 2(50) = 328 \text{ mm}$$

Pitch Circle diameter of the bolts

$$D_p = D + 2t + 2d + 12$$

$$200 + 2(14) + 2(21) + 12 = 282 \text{ mm}$$

Circumferential pitch of the bolts

$$P_c = \frac{\pi \times D_p}{n} = \frac{\pi \times 282}{8} = 110.7 \text{ mm}$$

For the joint to be leak proof,

the value of P_c should be b/w $20\sqrt{d}$ to $30\sqrt{d}$

d = diameter of bolt hole

$$d_1 = d + 3$$

$$= 21 + 3 = 24 \text{ mm}$$

$$20\sqrt{d_1} = 20\sqrt{24} = 97.9$$

$$30\sqrt{d_1} = 30\sqrt{24} = 140.9 \text{ [} P_c \text{ above } 20\sqrt{d_1} \text{ \& } 30\sqrt{d_1} \text{]}$$

therefore design is satisfactory

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3) A seamless pipe carries 2000 m^3 of steam per hour at a pressure of 1.2 N/mm^2 . The velocity of flow is 28 m/s . Assuming the tensile stress as 40 MPa , find the inside diameter of the pipe and its wall thickness.

Solution

$$Q = 2000 \text{ m}^3/\text{h} = 33.3 \text{ m}^3/\text{h}$$

$$P = 1.2 \text{ N/mm}^2$$

$$V = 28 \text{ m/s} = 1680 \text{ m/min}$$

$$\sigma_t = 40 \text{ MPa} = 40 \text{ N/mm}^2$$

inside diameter of pipe

$$D = 1.13 \sqrt{\frac{Q}{V}}$$

$$D = 1.13 \sqrt{\frac{33.3}{1680}}$$

$$= 0.159 = 160 \text{ mm}$$

Wall thickness of pipe

from table 8.2 $C = 3 \text{ mm}$

$$t = \frac{pD}{2} + C$$

$$= \frac{1.2 \times 160}{2 \times 40} + 3$$

$$= 5.4 \text{ mm} \approx 6 \text{ mm}$$

5) Design an axial flanged pipe joint for pipes of internal diameter 50mm subjected to a fluid pressure of 7N/mm^2 . The maximum tensile stress in the pipe materials is not to exceed 21MPa and in the bolts 28MPa .

$$D = 50\text{mm} \quad \text{or} \quad R = 25\text{mm}$$

$$p = 7\text{N/mm}^2$$

$$\sigma_t = 21\text{MPa} = 21\text{N/mm}^2$$

$$\sigma_{tb} = 28\text{MPa} = 28\text{N/mm}^2$$

$$t = R \left[\frac{\sigma_t + p}{\sigma_t - p} - 1 \right] = 25 \left[\frac{21+7}{21-7} - 1 \right] = 10.35 \approx 11\text{mm}$$

Assuming the width of packing as 10mm:

Outer diameter of packing

$$D_1 = D + 2 \times \text{width of packing} \\ = 50 + 2 \times 10 = 70\text{mm}$$

Force trying to separate the flanges

$$F = \frac{\pi}{4} (D_1)^2 p = \frac{\pi}{4} (70)^2 \times 7 = 26943\text{N}$$

Since the flange is secured by means of bolts

$$F_b = \frac{F}{2} = \frac{26943}{2} = 13471.5\text{N}$$

Let d_c = core diameter of bolt

load on each bolt (F_b)

$$13471.5 = \frac{\pi}{4} (d_c)^2 \times 28 = 21.99 (d_c)^2$$

$$(d_c)^2 = \frac{13471.5}{21.99} = 612.6$$

$$d_c = 24.7\text{mm} \approx 25\text{mm}$$

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Nominal diameter of bolts

$$d \text{ or } c \approx \underline{25}$$

$$0.84$$

$$0.85$$

$$29.4 \approx 30 \text{ mm}$$

Outer diameter of the flange

$$D_o = D + 2t + 4.6(D)$$

$$D_o = 50 + 2(11) + 4.6(30)$$

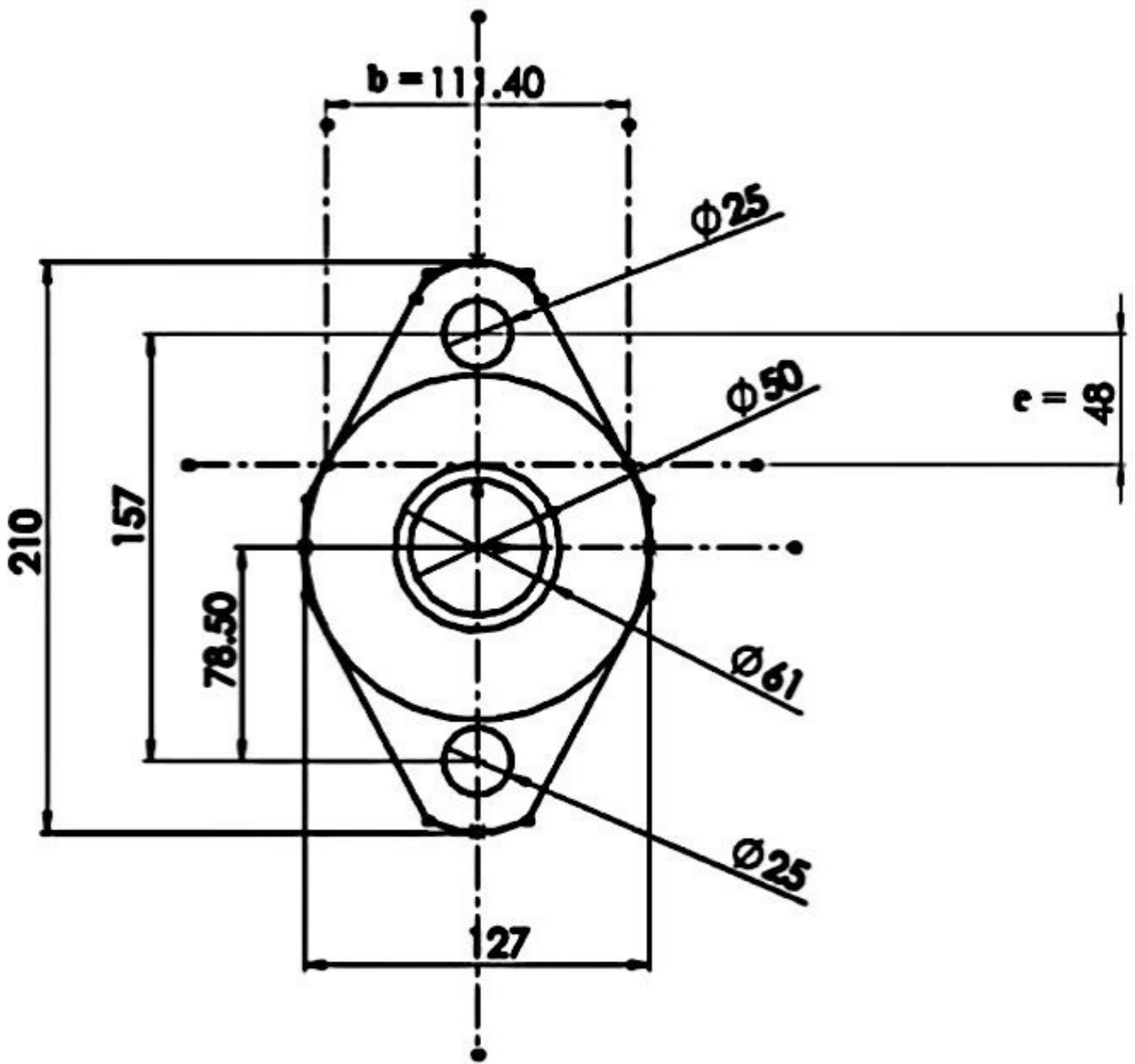
$$\approx 210 \text{ mm}$$

Pitch circle diameter of bolts

$$D_p = D_o - (3t + 20 \text{ mm})$$

$$\approx 210 - (3(11) + 20)$$

$$\approx 157 \text{ mm}$$



From the diagram above

$$b = 111.40 \text{ mm}$$

$$e = 48 \text{ mm}$$

Bending moment at Section $x-x$

$$\begin{aligned} \text{max } z \cdot F_b \times e &= ~~13471~~ 13471.5 \times 48 \text{ mm} \\ &= 646652 \text{ Nmm} \end{aligned}$$

and Section modulus

$$\begin{aligned} z &= \frac{1}{6} b (t_f)^2 = \frac{1}{6} \times 111.40 (t_f)^2 \\ &= 18.56 (t_f)^2 \end{aligned}$$

(max $z \cdot b \times z$)

$$\begin{aligned} 646652 &= 21 \times 18.55 (t_f)^2 \\ &= 389.76 (t_f)^2 \end{aligned}$$

$$t_f^2 = \frac{646652}{389.76} \quad \therefore t_f = \sqrt{1659.05} = 40.7 \approx 41 \text{ mm}$$