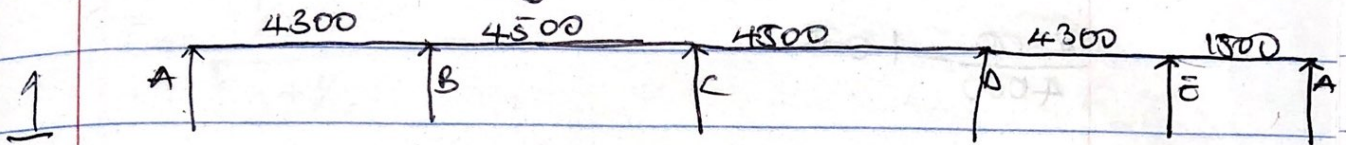


Assignment 2.



Assuming thickness = 150mm

$$F_{cu} = 25 \text{ N/mm}^2$$

$$F_y = 410 \text{ N/mm}^2$$

Slab loading

$$\text{Slab weight} = 0.15 \times 24 = 3.6 \text{ kN/m}^2$$

$$\text{Partition} = 1.0 \text{ kN/m}^2$$

$$\text{Finishes} = 1.2 \text{ kN/m}^2$$

$$\text{Total Gk} = 5.8 \text{ kN/m}^2$$

$$\text{D.L} = 1.4(5.8) + 1.6(3.0) = 13 \text{ kN/m}^2$$

Beam loading

$$\text{Self weight of beam} = 0.225 \times 0.6 \times 24 = 5.24 \text{ kN/m}^2$$

$$\text{Finishes} = 1.2 \text{ kN/m}^2$$

$$\text{Wall load} = 3 \times 3.47 = 10.41 \text{ kN/m}^2$$

$$\text{Total Gk} = 14.85$$

$$\text{D.L} = 1.4(14.85) = 20.79 \text{ kN/m}^2$$

$$\text{Load on beam in larger direction} = \frac{1}{2} w_b c (1 - \frac{c}{l})$$

$$k = \frac{c_y}{l_x}$$

$$\frac{4300}{4000} = 1.075$$

$$\frac{4500}{4000} = 1.125$$

$$\frac{1}{2} \times 13 \times 4.3 \left(1 - \frac{1}{3} \times 1.075^2\right) = 19.89 \text{ kN/m}^2$$

$$\frac{1}{2} \times 13 \times 4.5 \left(1 - \frac{1}{3} \times 1.125^2\right) = 21.55 \text{ kN/m}^2$$

Slab load on beam in shorter direction = $\frac{1}{3} w d c$

$$= \frac{1}{3} \times 13 \times 1.5 = 6.5 \text{ kN/m}^2$$

$$\text{Total load} = 19.89 + 20.79 = 40.68 \text{ kN/m}$$

$$= 21.55 + 20.79 = 42.34 \text{ kN/m}$$

$$= 6.54 + 20.79 = 27.29 \text{ kN/m}$$

Distribution factor

$$k_{ab} = 1$$

$$k_{ba} = \frac{\frac{1}{L_{BA}}}{\frac{1}{L_{BA}} + \frac{1}{L_{BC}}} = \frac{\frac{1}{4.3}}{\frac{1}{4.3} + \frac{1}{4.5}} = 0.51$$

$$k_{bc} = 1 - 0.51 = 0.49$$

$$k_{cb} = \frac{\frac{1}{L_{CB}}}{\frac{1}{L_{CB}} + \frac{1}{L_{CA}}} = \frac{\frac{1}{4.5}}{\frac{1}{4.5} + \frac{1}{4.5}} = 0.5$$

$$k_{ca} = 1 - 0.5 = 0.5$$

$$k_{dc} = 0.49$$

$$k_{de} = 0.51$$

$$k_{\text{so}} = \frac{\frac{1}{4} \cdot 3}{\frac{1}{4} \cdot 3 + \frac{1}{1005}} = 0.26$$

$$k_{\text{so}} = 1 - 0.26 = 0.79$$

$$k_{\text{so}} = 0$$

F. E. M.

$$U \cdot D \cdot L = \frac{wL^2}{12}$$

$$1) \frac{40 \cdot 68 \times 4 \cdot 3^2}{12} = 62.68 \text{ kNm}$$

$$2) \frac{42 \cdot 34 \times 4 \cdot 5^2}{12} = 70.45 \text{ kNm}$$

$$3) \frac{27 \cdot 29 \times 4 \cdot 5^2}{12} = 5.1 \text{ kNm}$$

	A	B	C	D	E	A'	
	AB	BA BC	CB CD	DC DE	ED EA	AE A'	
J.F	0 1	0.51 0.44	0.5 0.5	0.49 0.51	0.30 0.24	-2 0	
FEM	-62.68	62.68 -71.45	71.45 -71.45	71.45 -62.68	62.68 5.1	3.1	
OBM	-62.68	-8.77	0	8.77	5.758	-5 1	
BM	62.68	8.77	0	-8.77	-5.758	5 1	
DM	0	62.68	0 0	-4.30 -4.47	-4.49 -4.261	-5 10	
TM	2.235	31.38	2.15	2.15	2.49	-2.24 -2.55	-2.30
OBM	2.235	31.34	0	-7.49	-4.29	-21.305	
BM	-2.235	-31.34	0	7.49	4.29	21.305	
DM	0	2.235	0 0	3.67 3.82	1.25 3.54	213 0	
TM	2.44	-1.12	-7.69	1.84	0.63	1.41	10.66
OBM	-7.49	-1.12	-5.85	0.63	12.57	1.77	
BM	7.49	1.12	5.85	-0.63	-12.57	-1.77	
DM	0	7.49	0.57 0.55	2.43 2.93	-0.31 -0.32	-3.22 -4.29	-1.77 0
TM	0.29	3.40	1.42	0.28	1.47	1.64	-0.16 0.89
OBM	0.29	4.87	0.2	-0.17	-1.05	-4.65	
BM	-0.29	-4.87	-0.2	0.17	1.05	4.65	
DM	0	0.29	-2.48 -2.39	-0.06 -0.06	0.00	0.27 0.78	4.65 0
TM	0	22.88	-82.88	68.06 -69.05	72.06 -72.06	45.46 45.46	0

Moments

$$M_a = 0 \text{ kNm}$$

$$M_b = 82.88 \text{ kNm}$$

$$M_c = 69.06 \text{ kNm}$$

$$M_d = 72.06 \text{ kNm}$$

$$M_E = 45.47 \text{ kNm}$$

$$M_A' = 0 \text{ kNm}$$

Free moment

$$\text{For U.D.L} = \frac{wL^2}{8}$$

$$1) \frac{40.68 \times 4.3^2}{8} = 94.02 \text{ kNm}^2$$

$$2) \frac{42.34 \times 4.5^2}{8} = 107.17 \text{ kNm}^2$$

$$3) \frac{27.29 \times 1.5^2}{8} = 8.24 \text{ kNm}^2$$

Span moment

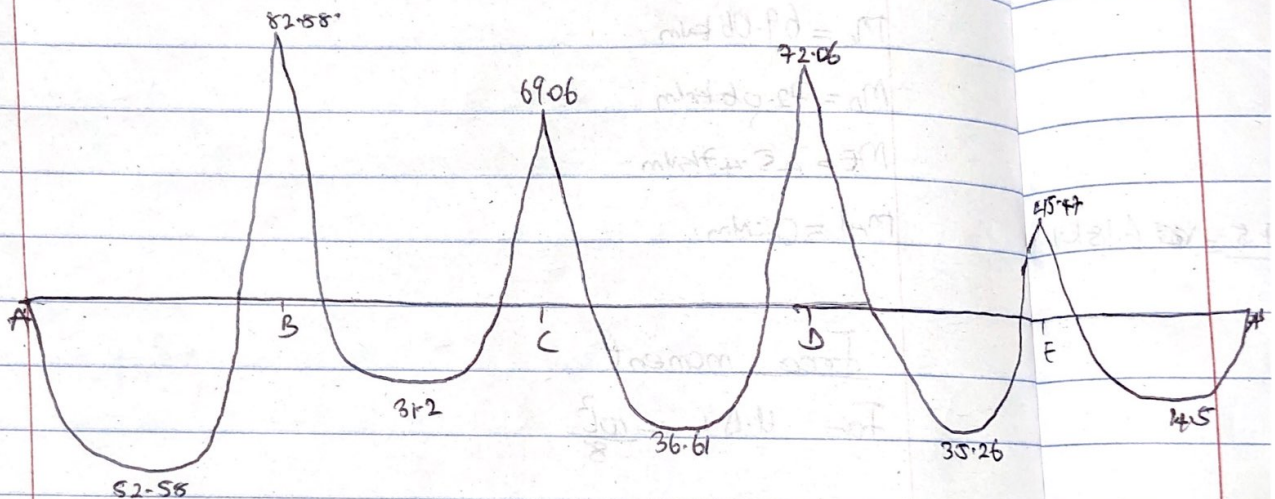
$$M_{ab} = M^F - \left(\frac{M_a + M_b}{2} \right) = 94.02 - \left(\frac{0 + 82.88}{2} \right) = 52.88 \text{ kNm}$$

$$M_{bc} = M^F - \left(\frac{M_b + M_c}{2} \right) = 107.17 - \left(\frac{82.88 + 69.06}{2} \right) = 31.2 \text{ kNm}$$

$$M_{CB} = MF - \left(\frac{M_C + M_D}{2} \right) = 107.17 - \left(\frac{69.06 + 72.06}{2} \right) = 36.61 \text{ kNm}$$

$$M_{DE} = MF - \left(\frac{M_D + M_E}{2} \right) = 94.02 - \left(\frac{72.06 + 45.47}{2} \right) = 35.26 \text{ kNm}$$

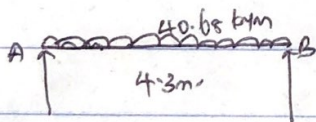
$$M_{EA} = MF - \left(\frac{M_E + M_A}{2} \right) = 8.24 - \left(\frac{45.47 + 0}{2} \right) = -14.5 \text{ kNm}$$



B.M.D.

Shear force:

For A



$$V_A = \frac{wl}{2} = V_B$$

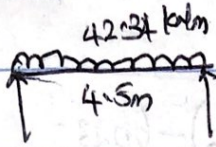
$$= \frac{40.68 \times 4.3}{2} = 87.462 \text{ kN}$$

$$V_{AB} = V_A + \left(\frac{M_A - M_B}{L} \right) = 87.462 + \left(\frac{0 - 82.88}{4.3} \right) = 68.19$$

$$V_{BA} = wl - V_{AB}$$

$$= (40.68 \times 4.3) - 68.19 = 106.73 \text{ kN}$$

For B



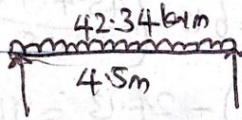
$$V_{BC} = \frac{wL}{2} = V_c$$

$$= \frac{42.34 \times 4.5}{2} = 95.27 \text{ kN}$$

$$V_{sc} = V_B + \left(\frac{M_B + M_C}{L} \right) = 95.27 + \left(\frac{82.68 + 69.06}{4.5} \right) = 129.03 \text{ kN}$$

$$V_{CB} = (42.34 \times 4.5) - 129.03 \\ = 61.5 \text{ kN}$$

For C



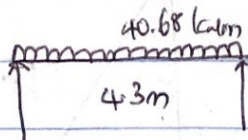
$$V_c = \frac{wL}{2} = V_D$$

$$= \frac{42.34 \times 4.5}{2} = 95.27 \text{ kN}$$

$$V_{cD} = 95.27 + \left(\frac{69.06 + 72.06}{4.5} \right) = 126.63 \text{ kN}$$

$$V_{DC} = (42.34 \times 4.5) - 126.63 = 63.19 \text{ kN}$$

For D



$$V_D' = \frac{wL}{2} = V_E$$

$$= \frac{40.68 \times 4.3}{2} = 87.46 \text{ kN}$$

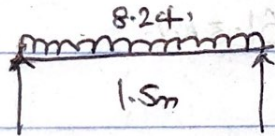
$$V_{DE} = V_D - \left(\frac{M_D + M_E}{L} \right) = 87.46 - \left(\frac{72.06 + 45.47}{4.3} \right) = 60.13 \text{ kN}$$

$$V_{00} = wL - V_{0E}$$

$$= (40.68 \times 4.3) - 60.13$$

$$= 114.79 \text{ kN}$$

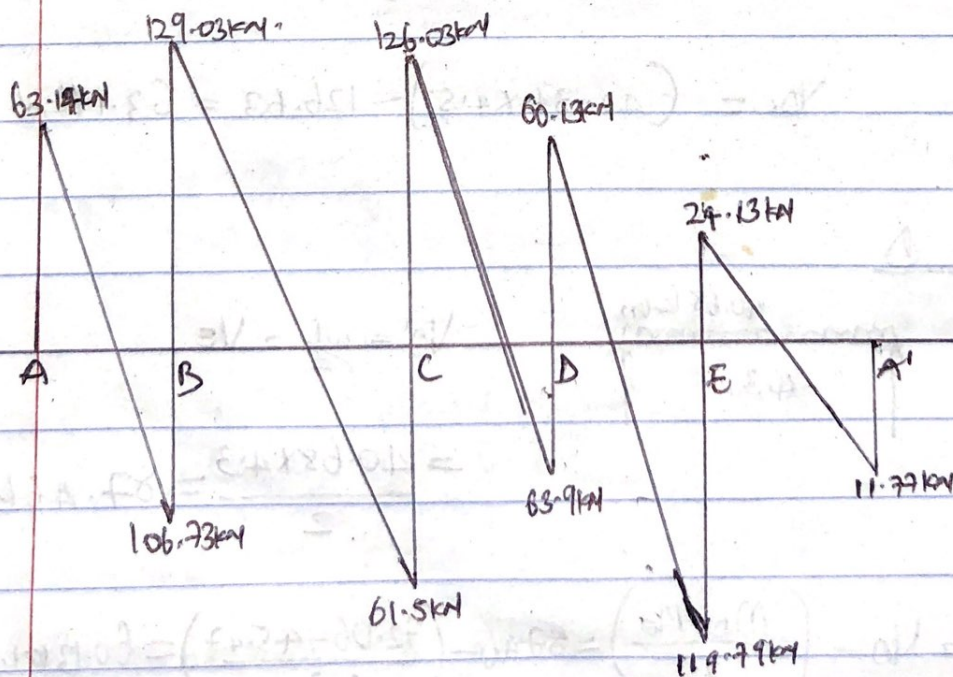
For E'



$$V_{E'} = \frac{wL}{2} = V_{A'} = \frac{8.24 \times 1.5}{2} = 6.18 \text{ kN}$$

$$V_{EA} = V_{E'} - \left(\frac{m_0 + m_A}{L} \right) = 6.18 - \left(\frac{45.47 + 0}{1.5} \right) = 24.13 \text{ kN}$$

$$V_{AE} = (8.24 \times 1.5) - 24.13 = 11.77 \text{ kN}$$



2)

Base design:

$$N = 1200 \text{ kN}$$

$$\text{width} = 25 - 410 \text{ N/mm}^2$$

$$F_b = 150 \text{ kN/m}^2$$

$$\text{Area of base required} = \frac{N \times 1.1}{A \times F_b} \quad A = 1.46$$

$$\frac{1200 \times 1.1}{1.46 \times 150} = 6.027 \text{ m}^2$$

$$1.46 \times 150$$

$$\sqrt{6.027} = 2.45 \text{ m} \approx 2.5$$

$$\text{Net pressure, } F_{\text{net}} = \frac{N \times 1.4}{B}$$

$$\frac{1200 \times 1.1}{3.5} - 24 \times 0.660 \times 1.4 = 505.824 \text{ kN/m}$$

$$\text{moment, } m = \frac{F_{\text{net}} l^2}{2}$$

where $l = \frac{1}{2}(B - h)$ ϕ = depth of base = 660

$$h = \frac{1}{2}(25 - 0.225) = 1.188$$

$$m = \frac{505.824 \times 1.14^2}{2} = 328.68 \text{ kNm}$$

$$d = h - \text{cover} - \frac{1}{2} \phi$$

$$= 660 - 50 - 10 = 600 \text{ mm}$$

$$k = \frac{M}{b^3 f_{cu}} = \frac{328.68 \times 10^6}{1000 \times 600^2 \times 25} = 0.032$$

$$P_u = 0.5 + \sqrt{0.25 + \frac{0.032}{0.9}} = 0.96 > 0.95$$

$$Z = k_{ad} = 0.95 \times 600 = 570 \text{ mm}$$

$$A_s = \frac{M}{0.95 f_{y2}} = \frac{328.68 \times 10^6}{0.95 \times 410 \times 570} = 480.44 \text{ mm}^2$$

Provide $\varnothing 25 @ 300 \%$ (1640).

Punching Shear.

$$\text{Column size} = 225 \times 450 \text{ mm}$$

$$F_{cu} f_y = 25 - 410 \text{ mm}$$

$$\text{Area footing} = 6.027 \text{ m}^2$$

$$\text{Size of footing} = 2500 \times 2500 \text{ mm}$$

$$q = \text{Net pressure} = 505.824 \text{ k/m}^2$$

$$\text{depth} = 600$$

$$\text{Critical section } \frac{d}{2} = 300$$

$$300 + 300 + 225 = 825 \text{ mm}$$

$$300 + 300 + 450 = 1050 \text{ mm}$$

$$\text{Shear force } V_u = q_n \times [\text{Area of footing} - (0.3 + d)^2]$$

$$= 505.824 [2.5 \times 2.5 - (0.3 + 0.6)^2]$$

$$V_u = 2751.68 \text{ kN}$$