

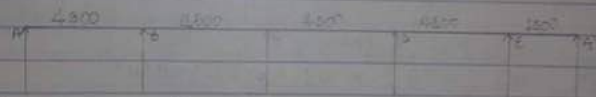
# CIVIL ENGINEERING

CVE 308

## STRUCTURAL DESIGN

### ASSIGNMENT TWO

#### QUESTION ONE



Assume that: Thickness = 150mm = 0.15m  
 $F_{ck} = 25\text{N/mm}^2$   
 $F_{yk} = 410\text{N/mm}^2$

#### Slab Loading

Slab weight =  $0.15 \times 24 = 3.6\text{KN/m}^2$   
Partition =  $1.0\text{KN/m}^2$   
Finishes =  $1.2\text{KN/m}^2$   
Total G.K. =  $5.8\text{KN/m}^2$   
Assume that O.K. =  $3.0'$   
 $D.L. = 1.4G.K. + 1.6Q.K.$   
 $= 1.4(5.8) + 1.6(3.0)$   
 $= 12.92\text{KN/m}^2 \approx 13\text{KN/m}^2$

## Beam loading

$$\text{Self weight of beam} = 0.225 \times 0.6 \times 24 = 3.24 \text{ kN/m}^2$$

$$\text{Screeding / finishes} = 1.2 \text{ kN/m}^2$$

$$\text{Wall} = 3.47 \times 3 = 10.41 \text{ kN/m}^2$$

$$\text{Total G.K.} = 14.85 \text{ kN/m}^2$$

$$D.L = 1.4 \text{ G.K.}$$

$$= 1.4 (14.85)$$

$$= 20.79 \text{ kN/m}^2 \approx 21 \text{ kN/m}^2$$

Sub loading on beam along shorter span

$$= \frac{1}{3} wlx$$

$$= \frac{1}{3} \times 13 \times 1.5$$

$$= 6.5 \text{ kN/m}^2$$

$$\text{Total load} = 6.5 + 21 = 27.5 \text{ kN/m}^2$$

Sub loading on beam along longer span

$$= \frac{1}{2} wlx (1 - \frac{1}{3} k^2)$$

$$k = \frac{l_y}{l_x}$$

$$= \frac{4.3}{4.0}$$

$$k^2 = \frac{4.3^2}{4.0^2}$$

$$= 1.16$$

$$= 1.016$$

$$= \frac{1}{2} \times 13 \times 4.3 \left(1 - \frac{1}{3} \times 1.016\right)$$

$$= 19.89 \text{ kN/m}^2$$

$$\text{Total load} = 19.89 + 21 = 40.89 \text{ kN/m}^2$$

$$\begin{aligned}
 k_2 &= 4000 \\
 &4000 \\
 &= 1.125
 \end{aligned}$$

$$\begin{aligned}
 &= \frac{1}{2} \times 13 \times 4.5 + \left(1 - \frac{1}{2}(1.125^2)\right) \\
 &= 21.53 \text{ kN/m}^2
 \end{aligned}$$

$$\text{Total Load} = 21.53 + 21 = 42.53 \text{ kN/m}^2$$

Distribution Factor

$$k_{AB} = 1$$

$$\begin{aligned}
 k_{BA} &= \frac{I_{LBA}}{I_{LBA} + I_{LBC}} = \frac{I_{4.3}}{I_{4.5} + I_{4.6}} \\
 &= 0.51
 \end{aligned}$$

$$\begin{aligned}
 k_{BC} &= 1 - 0.51 \quad k_{CB} = \frac{I_{4.5}}{I_{4.5} + I_{4.3}} = 0.49 \\
 &= 0.49
 \end{aligned}$$

$$\begin{aligned}
 k_{CB} &= \frac{I_{CB}}{I_{CB} + I_{CA}} = \frac{I_{4.5}}{I_{4.5} + I_{4.6}} \\
 &= 0.6
 \end{aligned}$$

$$\begin{aligned}
 k_{CA} &= \frac{I_{CA}}{I_{CA} + I_{CB}} = \frac{I_{4.6}}{I_{4.6} + I_{4.5}} \\
 &= 0.5
 \end{aligned}$$

$$\begin{aligned}
 k_{AC} &= \frac{I_{AC}}{I_{AC} + I_{AB}} = \frac{I_{4.5}}{I_{4.5} + I_{4.6}} \\
 &= 0.49
 \end{aligned}$$

$$\begin{aligned}
 k_{BE} &= \frac{I_{BE}}{I_{BE} + I_{BC}} = \frac{I_{4.6}}{I_{4.6} + I_{4.5}} \\
 &= 0.51
 \end{aligned}$$

$$K_{EA} = \frac{1/L_{EA}}{1/L_{EA} + 1/L_{EA'}} = \frac{1/4.3}{1/4.3 + 1/1.5} = 0.26$$

$$K_{EA'} = \frac{1/L_{EA'}}{1/L_{EA} + 1/L_{EA'}} = \frac{1/1.5}{1/4.3 + 1/1.5} = 0.74$$

$$K_{A'E} = 1$$

$$(FEM)_{AB} = -\frac{wL^2}{12} = -\frac{40.89 \times (4.3)^2}{12} = -63 \text{ kNm}$$

$$(FEM)_{BA} = \frac{wL^2}{12} = \frac{40.89 \times (4.3)^2}{12} = 63 \text{ kNm}$$

$$(FEM)_{BC} = -\frac{wL^2}{12} = -\frac{42.03 \times (4.5)^2}{12} = -71.8 \text{ kNm}$$

$$(FEM)_{CB} = \frac{wL^2}{12} = 71.8 \text{ kNm}$$

$$(FEM)_{CA} = -\frac{wL^2}{12} = -71.8 \text{ kNm}$$

$$(FEM)_{AC} = \frac{wL^2}{12} = 71.8 \text{ kNm}$$

$$(FEM)_{DE} = -\frac{wL^2}{12} = -63 \text{ kNm}$$

$$(FEM)_{ED} = \frac{wL^2}{12} = 63 \text{ kNm}$$

$$(FEM)_{EA} = \frac{-wL^2}{12} = \frac{-27.6 \times (1.5)^2}{12} = -5.2 \text{ kNm}$$

$$(FEM)_{AE} = \frac{wL^2}{12} = 5.2 \text{ kNm}$$

Joint Number	A	B		C		D		E		F
	AB	BA	BC	CB	CD	DC	DE	ED	EA	FE
DF	0	1	0.5	0.47	0.5	0.5	0.47	0.5	0.74	1
FEM	-6.5	6.5	-11.9	11.9	-11.9	11.9	-6.5	6.5	-5.2	5.2
DBM			-9.9		0		9.9		51.8	
EBM			9.9		0		-9.9		-51.8	
DM			4.9	4.5	0	0	4.5	4.4	-1.5	-42.7
TM	2.24	0	0	2.5	-2.5	-7.0	-1.5	-2.24	0	2.5
DBM			0		0		-1.5		-2.24	
EBM			0		0		1.5		2.24	
DM			0	0	0	0	0.67	0.62	0.58	1.65
TM	0	0	0	0	1.94	0	0.29	1.91	0	0.53
DBM			0		+1.54		0.29		1.81	
EBM			0		-1.54		-0.29		-1.19	
DM			0	0	-0.92	0.82	-0.14	-0.15	-0.31	0.96
TM	0	0	0	0	-0.46	0	-0.74	-0.44	-0.15	0
DBM			-0.46		-0.7		-0.51		-0.5	
EBM			0.46		0.7		0.51		0.5	
DM			+0.25	+0.23	0.35	0.35	0.29	0.24	0.29	0.55
TM	+0.25	0	+0.15	0	-0.15	0	+0.15	0	-0.15	0
Σ	0	22.98	-32.05	69.01	-69.05	12.05	-12.06	45.8	-45.84	0

### Moments

$$M_A = 0 \text{ kNm}$$

$$M_B = 92.55 \text{ kNm}$$

$$M_C = 69.06 \text{ kNm}$$

$$M_D = 72.06 \text{ kNm}$$

$$M_E = 45.41 \text{ kNm}$$

$$M_F = 0 \text{ kNm}$$

$$\text{Free Moment} = \frac{wL^2}{8}$$

$$\begin{aligned} 1) &= \frac{40.89 \times (4.3)^2}{8} \\ &= 94.51 \text{ kNm} \end{aligned}$$

$$\begin{aligned} 2) &= \frac{42.53 \times (4.5)^2}{8} \\ &= 107.65 \text{ kNm} \end{aligned}$$

$$\begin{aligned} 3) &= \frac{37.5 \times (1.5)^2}{8} \\ &= 7.75 \text{ kNm} \end{aligned}$$

### Span Moment

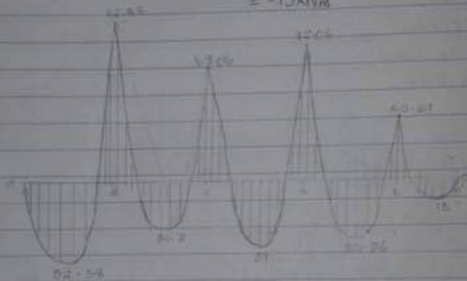
$$\begin{aligned} M_{AB} &= M^* \cdot \left( \frac{M_A + M_B}{2} \right) = 94.51 \cdot \left( \frac{0 + 92.55}{2} \right) \\ &= 52.56 \text{ kNm} \end{aligned}$$

$$\begin{aligned} M_{BC} &= M^* \cdot \left( \frac{M_B + M_C}{2} \right) = 107.65 \cdot \left( \frac{92.55 + 69.06}{2} \right) \\ &= 31.2 \text{ kNm} \end{aligned}$$

$$\begin{aligned} M_{CD} &= M^* \cdot \left( \frac{M_C + M_D}{2} \right) = 107.65 \cdot \left( \frac{69.06 + 72.06}{2} \right) \\ &= 37 \text{ kNm} \end{aligned}$$

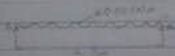
$$\begin{aligned} M_{DE} &= M^* \cdot \left( \frac{M_D + M_E}{2} \right) = 94.51 \cdot \left( \frac{72.06 + 45.41}{2} \right) \\ &= 35.26 \text{ kNm} \end{aligned}$$

$$M_{\text{cut}} = M^r - \left( \frac{M_a + M_a'}{2} \right) = 7.73 - \left( \frac{4.5 \cdot 4.7 + 0}{2} \right) = -15 \text{ kNm}$$



Shear Force

For A

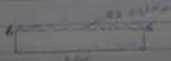


$$V_A = \frac{wL}{2} = \frac{20.99 \cdot 4.5}{2} = 47.5 \text{ kN} = V_A$$

$$V_{AB} = V_A + \left( \frac{M_A - M_B}{L} \right) = 47.5 + \left( \frac{0 - 22.58}{4.5} \right) = 66.7$$

$$V_{BA} = V_L - V_{AB} = (40.59 - 66.7) = -26.1 \text{ kN}$$

For B



$$V_B = \frac{wL}{2} = \frac{22.53 \cdot 4.7}{2} = 53.1 \text{ kN} = V_B$$

$$V_{BC} = V_B + \left( \frac{M_B + M_C}{L} \right) = 53.1 + \left( \frac{22.58 + 69.06}{4.5} \right) = 127.5 \text{ kN}$$

$$V_{CB} = V_L - V_{BC} = (22.53 - 127.5) = -105 \text{ kN}$$

For C



$$V_c = \frac{wL}{2} = \frac{42.53 \times 4.5}{2} = 95.7 \text{ kN}$$

$$V_{c0} = V_c + \left( \frac{M_c + M_D}{L} \right) = 95.7 + \left( \frac{69.06 + 12.06}{4.5} \right) = 127 \text{ kN}$$

$$V_{c1} = wL - V_{c0} = (42.53 \times 4.5) - 127 = 64.4 \text{ kN}$$



$$V_D = \frac{wL}{2} = \frac{40.89 \times 4.3}{2} = 88 \text{ kN}$$

$$V_{D0} = V_D + \left( \frac{M_D + M_C}{L} \right) = 88 + \left( \frac{12.06 + 45.47}{4.3} \right) = 60.7 \text{ kN}$$

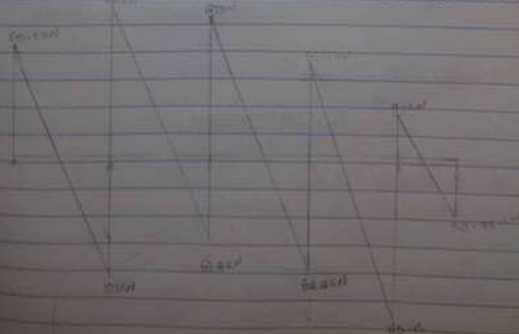
$$V_{D1} = wL - V_{D0} = (40.89 \times 4.3) - 60.7 = 110.13 \text{ kN}$$



$$V_E = \frac{wL}{2} = \frac{27.5 \times 1.5}{2} = 20.63 \text{ kN}$$

$$V_{E0} = V_E + \left( \frac{M_E + M_A}{L} \right) = 20.63 + \left( \frac{45.47 + 10}{1.5} \right) = 9.7 \text{ kN}$$

$$V_{E1} = wL - V_{E0} = (27.5 \times 1.5) - (9.7 \text{ kN}) = 30.95 \text{ kN}$$





## QUESTION TWO

Base Design

$$M = 1200 \text{ kNm}$$

$$\text{Strength} = 80-410 \text{ N/mm}^2$$

$$\text{BBC} = 100 \times 100 \text{ mm}^2$$

$$\lambda = 1.46$$

$$\text{Area of Base Required} = \frac{M \times 1.1}{A \times \text{BBC}} = \frac{1200 \times 1.1}{1.46 \times 100}$$
$$= 6.021 \text{ m}^2$$

$$\sqrt{6.021} = 2.45 \text{ m} \approx 2.5 \text{ m}$$

$$\text{Net Pressure, } I_{\text{net}} = \frac{M \times 1.1}{B} = \frac{1200 \times 1.1}{2.5}$$

$$= 528 = (84 \times 0.660 \times 1.4)$$

$$= 500.824 \text{ kNm}$$

$$\text{Moment, } M = I_{\text{net}} \times L^2$$

$$\text{where } L = \frac{1}{2} (B - b)$$

$$L = \frac{1}{2} (2.5 - 0.660)$$

$$= 1.175 \text{ m} \approx 1.14 \text{ m}$$

$$M = \frac{500.824 \times (1.14)^2}{2}$$

$$= 323.65 \text{ kNm}$$

$$d = n - \text{cover} - \frac{1}{2} \phi$$

$$= 660 - 00 - 10 = 650 \text{ mm}$$

$$n = \frac{M}{k d^2 f_{ck}} = \frac{323.65 \times 10^3}{1000 \times 650^2 \times 40}$$
$$= 0.032$$

$$I_a = 0.5 + \sqrt{0.25 + \frac{2.03^2}{8.9}}$$

$$= 0.96 (\approx 0.96)$$

$$Z = I_a d = 0.96 \times 600$$

$$= 576 \text{ mm}$$

$$Z_o = \frac{\pi}{0.955 \times Z} = \frac{0.25 \times 10^6}{0.96 \times 410 \times 610}$$

$$= 1470.44 \text{ mm}^3$$

Provide 4R30 @ 300 Yc (A = 1640 mm<sup>3</sup>)

Punching Shear

Column size = 225 x 450 mm

$f_{ck}/f_y = 80 - 210 \text{ mm}^2$

Area footing = 6.071 m<sup>2</sup>

Size of footing = 2000 x 2000

$q_u$  Net Pressure = 505.824 kN/m<sup>2</sup>

Depth = 600

$$\text{Critical Section} = \frac{d}{2} = \frac{600}{2}$$

$$= 300$$

$$300 + 300 + 225 = 825 \text{ mm}$$

$$300 + 300 + 450 = 1050 \text{ mm}$$

$$\text{Shear Force } V_u = q_u \times (\text{Area Footing} - (0.3 + d)^2)$$

$$= 505.824 \times (6.071 - (0.3 + 0.6)^2)$$

$$V_u = 2751.63 \text{ kN}$$

$$\text{Normal Shear Stress } \tau_v = \frac{V_u}{b d} = \frac{2751.63}{(2 \times 0.25 \times 0.6) \times 600}$$

$$\tau_v = 7.883 \text{ N/mm}^2$$

### Permissible Shear Stress

$$\tau_c = K_b \times \tau_c$$

$$K_b = (0.5 + \phi_c)$$

$\phi_c$  = Ratio of longer to shorter sides

$$\tau_c = 0.80 \sqrt{T_u}$$

$$K_b = 1$$

$$\tau_c = 0.80 \sqrt{75}$$

$$= 1.80 \text{ N/mm}^2$$

$$T_u \approx \tau_c$$

$\therefore$  Shear assumed to be OK

Check for TB with actual footing size

Max Depth of concrete =  $84 \text{ N/mm}^2$

$$\therefore \text{ " " Soil} = 1.091 \times 10^6 \text{ N/mm}^2$$

$$\text{Actual footing } q = (1700 \times 2.5 \times 2.50 + 0.24 \times 0.60)$$

$$[1.091 \times 10^6 \times 0.24]$$

$$= 814.9 \text{ N/mm}^2$$