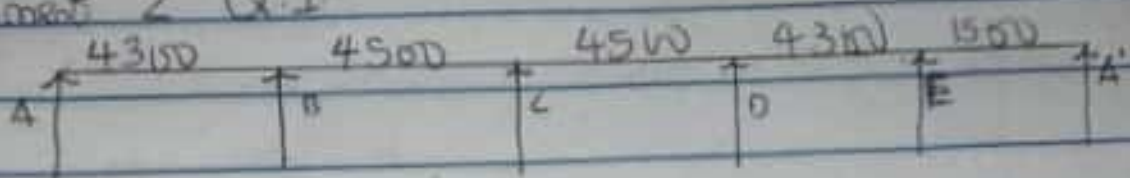


## Assignment 2 Q.1



Assuming thickness: 150mm

$$f_{cu} = 25 \text{ N/mm}^2$$

$$f_y = 410 \text{ N/mm}^2$$

### Slab loading

$$\text{Slab weight} = 0.15 \times 24 = 3.6 \text{ kN/m}^2$$

$$\text{Partition} = 1.0 \text{ kN/m}^2$$

$$\text{finishes} = 1.2 \text{ kN/m}^2$$

$$\text{Total G.k} = 5.8 \text{ kN/m}^2$$

$$\text{D.L} = 1.4(5.8) + 1.6(3.0) = 13 \text{ kN/m}^2$$

*assuming for column*

### Beam loading

$$\text{Self wt of beam} = 0.225 \times 0.6 \times 24 = 3.24 \text{ kN/m}^2$$

$$\text{finishes} = 1.2 \text{ kN/m}^2$$

$$\text{Wall load} = 3 \times 3.47 = 10.41 \text{ kN/m}^2$$

$$\text{Total G.k} = 14.85$$

$$\text{D.L} = 1.4(14.85) = 20.79 \text{ kN/m}^2$$

Slab load on beam in longer direction =  $\frac{1}{2} w l_x (1 - \frac{1}{3} \alpha^2)$

$$k = \frac{l_y}{l_x}$$

$$\frac{4300}{4000} = 1.075$$

$$4000$$

$$\frac{4500}{4000} = 1.125$$

$$4000$$

$$\frac{1}{2} \times 13 \times 4.3 \left( 1 - \frac{1}{3} \times (1.075)^2 \right) = 19.89 \text{ kN/m}^2$$

$$\frac{1}{2} \times 13 \times 4.5 \left( 1 - \frac{1}{3} \times (1.125)^2 \right) = 21.55 \text{ kN/m}^2$$

Slab load on beam in shorter direction =  $\frac{1}{3} w l_x$   
 $= \frac{1}{3} \times 13 \times 1.5 = 6.5 \text{ kN/m}^2$

$$\text{Total load} = 19.89 + 20.79 = 40.68 \text{ kN/m}$$

$$= 21.55 + 20.79 = 42.34 \text{ kN/m}$$

$$= 6.5 + 20.79 = 27.29 \text{ kN/m}$$

Distribution factor

$$k_{BA} = 1$$

$$k_{BA} = \frac{1}{k_{BA} + 1} = \frac{1}{1 + 3} = 0.51$$

$$\frac{1}{k_{BA} + 1} = \frac{1}{1 + 3}$$

$$k_{BC} = 1 - 0.51 = 0.49$$

$$k_{CB} = \frac{\frac{1}{4} \cdot 5}{\frac{1}{4} \cdot 5 + \frac{1}{4} \cdot 5} = 0.5$$

$$k_{CA} = 1 - 0.5 = 0.5$$

$$k_{DC} = 0.49$$

$$k_{DE} = 0.51$$

$$k_{ED} = \frac{\frac{1}{4} \cdot 3}{\frac{1}{4} \cdot 3 + \frac{1}{4} \cdot 5} = 0.26$$

$$k_{EA} = 1 - 0.26 = 0.74$$

$$k_{AE} = 0$$

F.E.M

$$= \frac{wL^2}{12}$$

$$1) \frac{40.68 \times 4.3^2}{12} = 62.68 \text{ kN/m}$$

$$2) \frac{42.34 \times 4.5^2}{12} = 71.49 \text{ kN/m}$$

$$3) \frac{27.29 \times 1.5^2}{12} = 5.1 \text{ kN/m}$$



	A	B	C	D	E	A'
	AB	BA BC	CB CD	DC DE	ED EA	AA'
D.F	0 1	0.5/0.44	0.5 0.5	0.44 0.51	0.44 0.74	3 0
FEM	-62.68	62.68 -71.45	71.45 -71.45	71.45 -62.68	62.68 51	51
OBM	-62.68	-8.77	0	8.77	57.58	-51
BM	62.68	8.77	0	-8.77	-57.58	51
DM	0 62.68	4.97 4.30	0 0	-4.30 -4.97	-4.97 -4.261	-51 0
TM	2.235	31.34 0	2.15 -2.15	0 -7.49	-2.24 -2.55	-21.305
OBM	2.235	31.34	0	-7.49	-4.79	-21.305
BM	-2.235	-31.34	0	7.49	4.79	21.305
DM	0 -2.235	-15.98 -15.56	0 0	3.67 3.82	1.25 3.54	21.3 0
TM	-7.49	-1.12 0	-7.69 1.34	0 0.63	1.91 10.56	1.77
OBM	-7.49	-1.12	-5.85	0.63	12.57	1.77
BM	7.49	1.12	5.85	-0.63	-12.57	-1.77
DM	0 7.49	0.57 0.55	2.43 2.43	-0.31 -0.32	-3.22 -9.24	-1.77 0
TM	0.24	3.40 1.47	0.28 -0.10	1.47 -1.64	-0.16 -0.19	-4.65
OBM	0.24	4.87	0.12	-0.17	-1.05	-4.65
BM	-0.24	-4.87	-0.12	0.17	1.05	4.65
DM	0 -0.24	-2.48 -2.39	-0.06 -0.06	0.08 0.09	0.21 0.78	4.65 0
Σ	= 0	22.88 -42.88	69.06 -69.05	72.06 -72.06	45.44 -45.46	0

Moments

$$M_a = 0 \text{ kNm}$$

$$M_b = 82.88 \text{ kNm}$$

$$M_c = 69.06 \text{ kNm}$$

$$M_d = 72.06 \text{ kNm}$$

$$M_E = 45.47 \text{ kNm}$$

$$M_{A'} = 0 \text{ kNm}$$

Free moment

$$\text{for U.D.L} = \frac{wL^2}{8}$$

$$1.) \frac{40.68 \times 4.3^2}{8} = 94.02 \text{ kNm}^2$$

$$2.) \frac{42.34 \times 4.5^2}{8} = 107.17 \text{ kNm}^2$$

$$3.) \frac{27.29 \times 1.5^2}{8} = 8.24 \text{ kNm}^2$$

Span moment

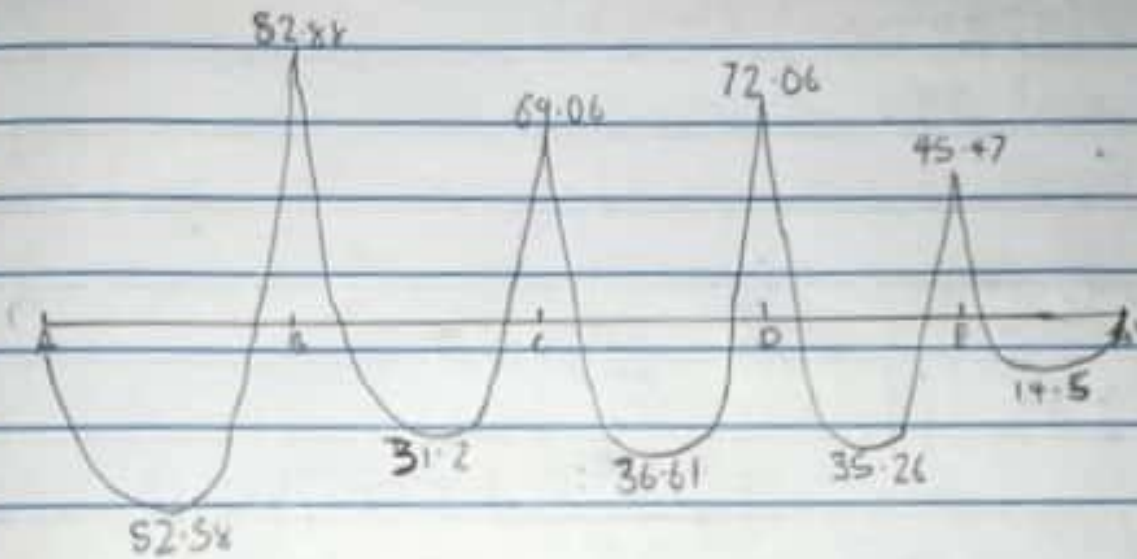
$$M_{ab} = M^f - \left( \frac{M_a + M_b}{2} \right) = 94.02 - \left( \frac{0 + 82.88}{2} \right) = 52.58 \text{ kNm}$$

$$M_{bc} = M^f - \left( \frac{M_b + M_c}{2} \right) = 107.17 - \left( \frac{82.88 + 69.06}{2} \right) = 31.21 \text{ kNm}$$

$$M_{CD} = M^F - \left( \frac{M_C + M_D}{2} \right) = 107.17 - \left( \frac{69.06 + 72.06}{2} \right) = 36.61 \text{ kNm}$$

$$M_{DE} = M^F - \left( \frac{M_D + M_E}{2} \right) = 94.02 - \left( \frac{72.06 + 45.47}{2} \right) = 35.26 \text{ kNm}$$

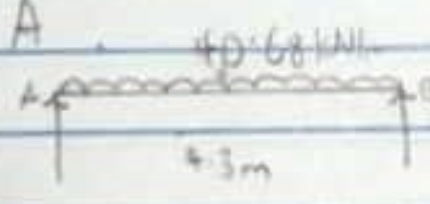
$$M_{EA'} = M^F - \left( \frac{M_E + M_{A'}}{2} \right) = 8.24 - \left( \frac{45.47 + 0}{2} \right) = -14.5 \text{ kNm}$$



B.M.D

Shear force

For A



$$V_A = \frac{wL}{2} = V_B$$

$$= \frac{40.68 \times 4.3}{2} = 87.462 \text{ kN}$$

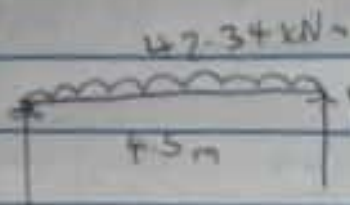
$$V_{AB} = V_A + \left( \frac{M_A - M_B}{L} \right) = 87.462 + \left( \frac{0 - 82.88}{4.3} \right) = 68.19$$

$$V_{BA} = wL - V_{AB}$$

$$= (40.68 \times 4.3) - 68.19 = 106.73 \text{ kN}$$



for B

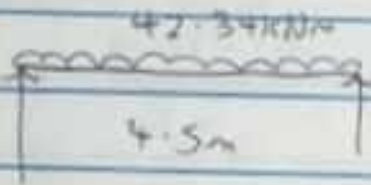


$$V_{Bc} = \frac{wl}{2} = V_c$$
$$= \frac{42.34 \times 4.5}{2} = 95.27 \text{ kN}$$

$$V_{Bc} = V_{Bc} + \left( \frac{M_{Bc} - M_{Ac}}{L} \right) = 95.27 + \left( \frac{82.68 + 69.06}{4.5} \right) = 129.03 \text{ kN}$$

$$V_{cB} = (42.34 \times 4.5) - 129.03$$
$$= 61.5 \text{ kN}$$

for C



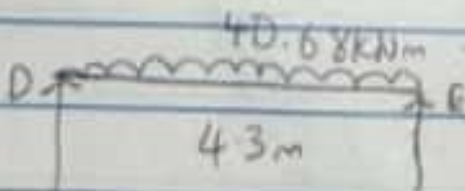
$$V_{cD} = \frac{wl}{2} = V_D$$

$$= \frac{42.34 \times 4.5}{2} = 95.27 \text{ kN}$$

$$V_{cD} = 95.27 + \left( \frac{69.06 + 72.06}{4.5} \right) = 126.63 \text{ kN}$$

$$V_{Dc} = (42.34 \times 4.5) - 126.63$$
$$= 63.19 \text{ kN}$$

for D



$$V_{D'E} = \frac{wl}{2} = V_E$$

$$= \frac{40.68 \times 4.3}{2} = 87.46 \text{ kN}$$

$$V_{DE} = V_D - \left( \frac{M_D + M_E}{L} \right)$$

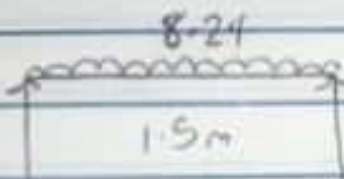
$$= 87.46 - \left( \frac{72.06 + 45.47}{4.3} \right) = 60.13 \text{ kN}$$

$$V_{ED} = W_L = V_{DE}$$

$$= (40.68 \times 4.3) - 60.13$$

$$= 114.79 \text{ kN}$$

for E



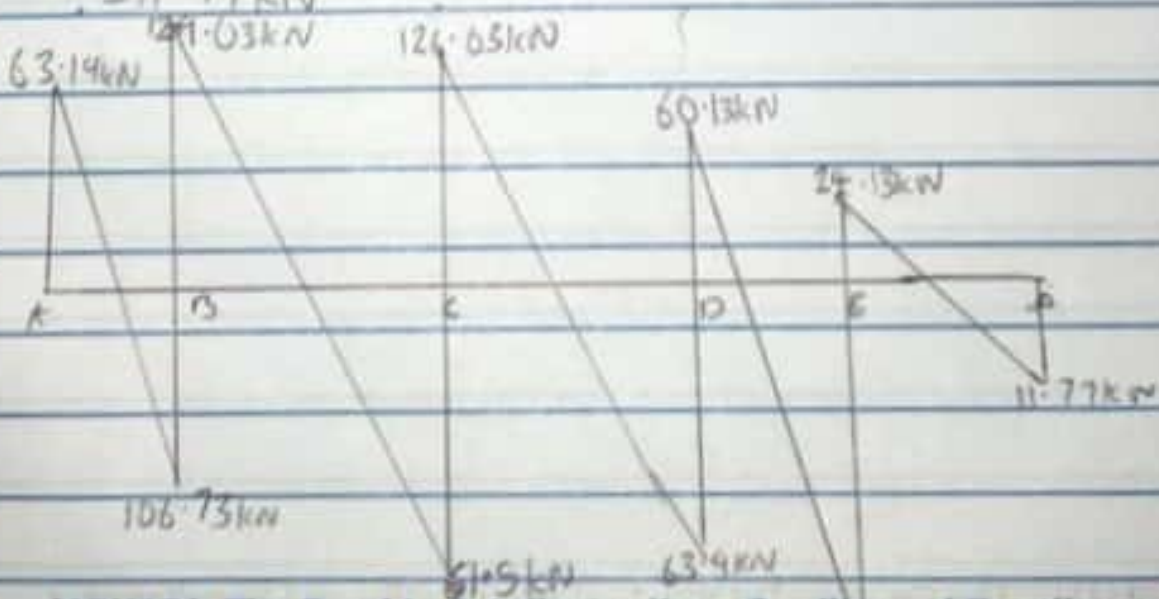
$$V_{E'} = \frac{wL}{2} = V_{D'}$$

$$= \frac{8.24 \times 1.5}{2} = 6.18 \text{ kN}$$

$$V_{E'A'} = V_{E'} - \left( \frac{M_E + M_{A'}}{L} \right) = 6.18 - \left( \frac{45.47 + 0}{1.5} \right) = 24.13 \text{ kN}$$

$$V_{A'E} = (8.24 \times 1.5) - 24.13$$

$$= 11.77 \text{ kN}$$



(ABUAD), The Road to Intellectualism, Quality and Excellence



# Assignment 2 No 2

Base design

$$N = 1200 \text{ kN}$$

$$\text{Strength} = 25 - 410 \text{ N/mm}^2$$

$$F_b = 150 \text{ kN/m}^2$$

$$\text{Area of base } a_{\text{req}} = \frac{N \times 1.1}{\lambda \times F_b} \quad \lambda = 1.46$$

$$\frac{1200 \times 1.1}{1.46 \times 150} = 6.027 \text{ m}^2$$

$$1.46 \times 150$$

$$\sqrt{6.027} = 2.45 \text{ m} \approx 2.5$$

$$\text{Net pressure, } F_{\text{net}} = \frac{N \times 1.1}{B}$$

$$\frac{1200 \times 1.1}{2.5} = 24 \times 0.660 \times 1.1$$

$$= 505.824 \text{ kN/m}$$

$$\text{Moment, } M = \frac{F_{\text{net}} l^2}{2}$$

$$\text{where } l = \frac{1}{2}(B - h) \quad \phi = \text{depth of base} = 660$$

$$l = \frac{1}{2}(2.5 - 0.225) = 1.138 \approx 1.14 \text{ m}$$

$$M = \frac{505.824 \times 1.14^2}{2} = 328.68 \text{ kNm}$$

$$d = h - \text{cover} - \frac{1}{2} \phi$$

$$= 660 - 50 - 10 = 600 \text{ mm}$$

$$k = \frac{M}{bd^2k_u} = \frac{328.68 \times 10^6}{1000 \times 600^2 \times 25} = 0.037$$

$$R_u = 0.5 + \sqrt{0.25 + \frac{0.037}{0.9}} = 0.967 > 0.95$$

$$z = \text{lad} = 0.95 \times 600 = 570 \text{ mm}$$

$$A_s = \frac{M}{0.95 f_y z} = \frac{328.68 \times 10^6}{0.95 \times 410 \times 570} = 1480.44 \text{ mm}^2$$

Provide  $725 \text{ @ } 300 \text{ i/c } (1640)$

Punching Spec

$$\text{Column size} = 225 \times 450 \text{ mm}$$

$$P_u f_y = 25 - 410 \text{ mm}$$

$$\text{Area footing} = 6.027 \text{ m}^2$$

$$\text{Size of footing} = 2500 \times 2500$$

$$q_u, \text{ Net pressure} = 505.824 \text{ kN/m}^2$$

$$\text{depth} = 600$$

$$\text{critical section, } \frac{d}{2} = 300$$

$$300 + 300 + 225 = 825 \text{ mm}$$

$$300 + 300 + 450 = 1050 \text{ mm}$$

$$\begin{aligned} \text{Pres force } V_u &= q_u \times [\text{Area of footing} - (0.3 + d)^2] \\ &= 505.824 [2.5 \times 2.5 - (0.3 + 0.6)^2] \\ V_u &= 2781.68 \text{ kN} \end{aligned}$$



Actual shear stress  $\tau_v = \frac{V_u}{bd}$

$b =$  perimeter of critical section

$d =$  effective span/depth

$$\tau_v = \frac{2751.67 \times 10^3}{(2 \times (825) + 2(1050)) \times 600}$$

$$\tau_v = 1.223 \text{ N/mm}^2$$

Permissible shear stress

$$\tau_c' = k_s \times \tau_c$$

$k_s = (0.5 + B_c)$  but not greater than 1

$B_c =$  Ratio of smaller to larger side of column

$$\tau_c = 0.25 \sqrt{f_{ck}}$$

$$k_s = 1$$

$$\tau_c' = 0.25 \sqrt{25} = 1.25 \text{ N/mm}^2$$

$$\tau_v = 1.223 \text{ N/mm}^2$$

$$\tau_v \leq \tau_c'$$

Hence depth assumed is ok ✓

Checking for  $f_b$  with actual size of footing

Unit weight of concrete =  $24 \text{ kN/m}^3$

Unit weight of soil =  $1.091 \times 10^{-6} \text{ kN/m}^3$

Actual pressure footing below

$$q = (1200 / (2.5 \times 2.5)) + (24 \times 0.660) + (1.091 \times 10^{-6} \times 0.660)$$

$$q = 214.94 \text{ kN/m}^2$$