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ABSTRACT

The permanent-magnet synchronous machine (PMSM) drive is one of the best choices for a full range of motion control applications. For example, the PMSM is widely used in robotics, machine tools, actuators, and it is being considered in high-power applications such as industrial drives and vehicular propulsion. It is also used for residential/commercial applications. The PMSM is known for having low torque ripple, superior dynamic performance, high efficiency and high power density. Section 1 deals with the introduction of PMSM and how it is evolved from synchronous motors. Section 2 briefly discusses about the types of PMSM. Section 3 tells about the assumptions in PMSM for modeling of PMSM and it derives the equivalent circuit of PMSM. In Section 4, permanent magnet synchronous motor drive system is briefly discussed with explanation of each block in the systems. Section 5 reveals about the control techniques of PMSM like scalar control, vector control and simulation of PMSM driven by field-oriented control using fuzzy logic control with space vector modulation for minimizing torque ripples.

INTRODUCTION

The electric motors are electromechanical machines, which are used for the conversion of electrical energy into mechanical energy. The foremost categories of AC motors are asynchronous and synchronous motors. The asynchronous motors are called singly excited machines, that is, the stator windings are connected to AC supply whereas the rotor has no connection from the stator or to any other source of supply. The power is transferred from the stator to the rotor only by mutual induction, owing to which the asynchronous motors are called as induction machines.

The synchronous motors require AC supply for the stator windings and DC supply for the rotor windings. The motor speed is determined by the AC supply frequency and the number of poles of the synchronous motor, the rotor rotates at the speed of the stator revolving field at synchronous speed, which is constant. The variations in mechanical load within the machine's rating will not affect the motor's synchronous speed [1].

One of the types of synchronous motor is the PMSM. The PMSM consists of conventional three phase windings in the stator and permanent magnets in the rotor. The purpose of the field windings in the conventional synchronous machine is done by permanent magnets in PMSM. The conventional synchronous machine requires AC and DC supply, whereas the PMSM requires only AC supply for its operation. One of the greatest advantages of PMSM over its counterpart is the removal of dc supply for field excitation as discussed in [2].

The development of PMSM has happened due to the invention of novel magnetic materials and rare earth materials. PMSM give numerous advantages in scheming recent motion management systems. Energy efficient PMSM are designed due to the availability of permanent magnet materials of high magnetic flux density.

In synchronous motors the rotor rotates at the speed of stator revolving field. The speed of the revolving stator field is called as synchronous speed. The synchronous speed (ω_s) can be found by the frequency of the stator input supply (f_s), and the number of stator pole pairs (p). The stator of a three phase synchronous motor consists of distributed sine three phase winding, whereas the rotor consists of the same number of p -pole pairs as stator, excited by permanent magnets or a separate DC supply source as given in [3].

When the synchronous machine is excited with a three phase AC supply, a magnetic field rotates at synchronous speed develops in the stator. The synchronous speed of this rotating magnetic field is shown by the Eq. (1).

$$N=(120f_s)/P \text{ rpm.....Eq (1)}$$

where N, synchronous speed, f_s , frequency of AC supply in Hz; P, number of poles; p, pole pairs and it is given by $(P/2)$.

Types of PMSM

The PMSM are classified based on the direction of field flux are as follows,

1. Radial field
2. Axial field

In radial field, the flux direction is along the radius of the machine. The radial field permanent magnet motors are the most commonly used. In axial field, the flux direction is parallel to the rotor shaft. The axial field permanent magnet motors are presently used in a variety of numerous applications because of their higher power density and quick acceleration.

Modeling of PMSM

For proper simulation and analysis of the system, a complete modelling of the drive model is essential. The motor axis has been developed using d-q rotor reference frame theory as shown in Figure 5 , as given [5]. At any particular time t, the rotor reference axis makes an angle θ_r with the fixed stator axis and the rotating stator mmf creates an angle α with the rotor d axis. It is viewed that at any time t, the stator mmf rotates at the same speed as that of the rotor axis.

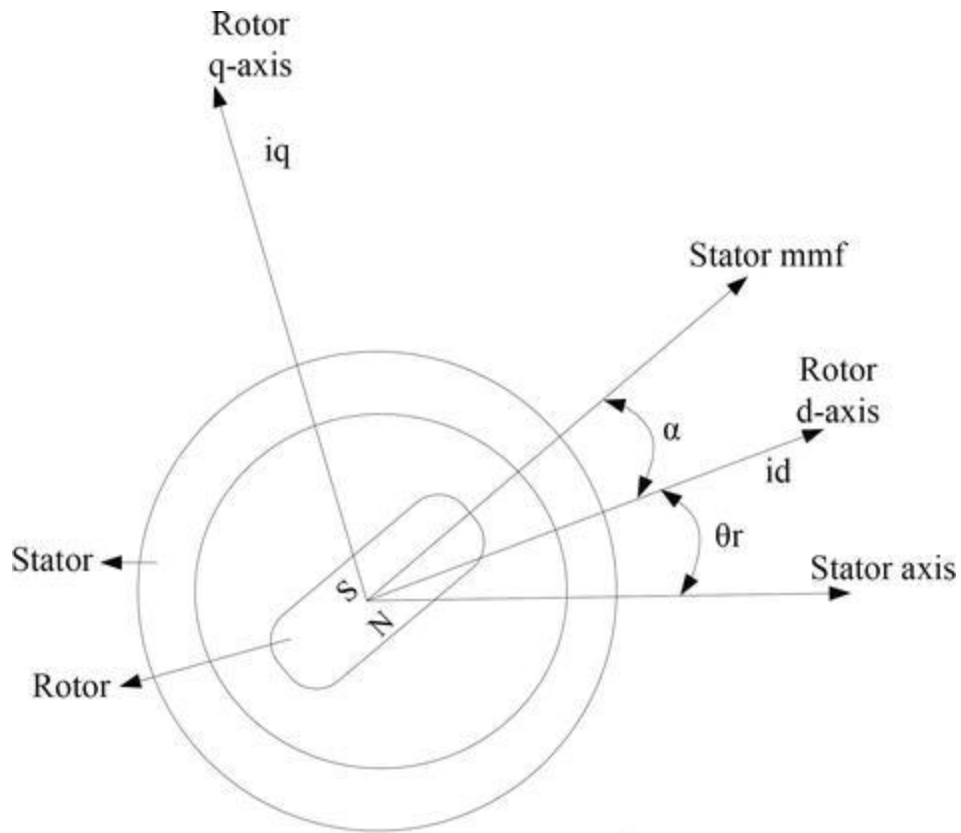


Figure 5. Motor axis.

The required assumptions are obtained for the modelling of the PMSM without damper windings.

1. Saturation is neglected.
2. Induced EMF is sinusoidal in nature.
3. Hysteresis losses and Eddy current losses are negligible.
4. No field current dynamics.

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Voltage equations from the model are given by,

$$V_q = R_s i_q + \omega_r \lambda_d + \rho \lambda_q \quad (3)$$

$$V_d = R_s i_d - \omega_r \lambda_q + \rho \lambda_d \quad (4)$$

Flux linkages are given by,

$$\lambda_q \frac{1}{2} L_{qiq} \quad (5)$$

$$\lambda_q \frac{1}{2} L_{qiq} \text{ } \rho \text{ } \lambda_f \quad (6)$$

Substituting Eq. (5) and Eq. (6) into Eq. (3) and Eq. (4)

$$V_q \frac{1}{2} R_{siq} \text{ } \rho \text{ } \omega_r \delta L_{did} \text{ } \rho \text{ } \lambda_f \text{ } \rho \text{ } \rho L_{did} \quad (7)$$

$$V_d \frac{1}{2} R_{sid} - \omega_r L_{qiq} \text{ } \rho \text{ } \delta L_{did} \text{ } \rho \text{ } \lambda_f \text{ } \rho \quad (8)$$

Arranging Eq. (7) and Eq. (8) in matrix form,

$$V_q V_d = R_s + \rho L_q \omega_r L_d - \omega_r L_q R_s + \rho L_d i_{qid} + \omega_r \lambda_f \rho \lambda_f \text{ Eq9}$$

The developed torque motor is being given by,

$$T_e = 3/2 P \lambda_d i_{q} - \lambda_q i_{d} \dots \text{ Eq10}$$

The mechanical torque equation is,

$$T_e = T_L + B \omega_m + J d \omega_m / dt \dots \text{ Eq11}$$

Solving for the rotor mechanical speed form..... Eq. (11)

$$\omega_m = \int (T_e - T_L - B \omega_m) / J dt \dots \text{ Eq12}$$

and

$$\omega_m = \omega_r / 2 P \text{ Eq13}$$

In the above equations ω_r is the rotor electrical speed, ω_m is the rotor mechanical speed.

Parks transformation and dynamic d-q modeling

The dynamic d-q modelling of the system is used for the study of motor during transient state and as well as in the steady state conditions. It is achieved by converting the three phase voltages and currents to d-qo axis variables by using the Parks transformation.

Converting the phase voltages variables V_{abc} to V_{dqo} variables in rotor reference frame axis are illustrated in the equations,

$$V_d = \frac{2}{3} \cos\theta_r V_a - \frac{2}{3} \sin\theta_r V_b - \frac{2}{3} \cos\theta_r V_c$$

$$V_q = \frac{2}{3} \sin\theta_r V_a + \frac{2}{3} \cos\theta_r V_b - \frac{2}{3} \sin\theta_r V_c$$

$$V_o = \frac{1}{3} (V_a + V_b + V_c)$$

....Eq14

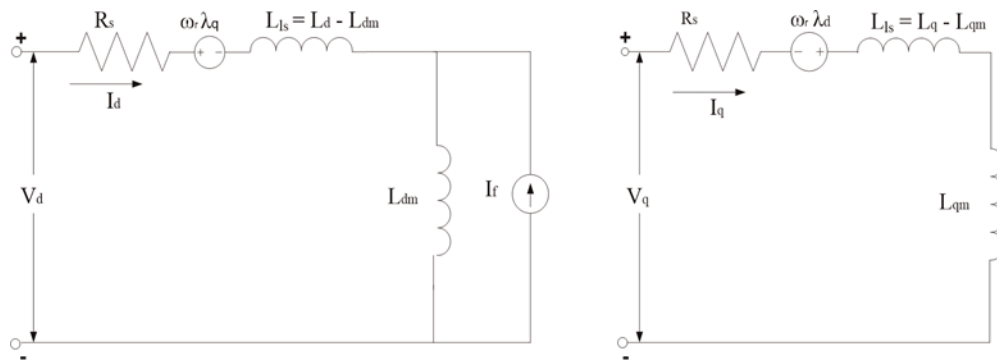
Convert V_{dqo} to V_{abc}

$$V_a = \frac{2}{3} \cos\theta_r V_d - \frac{2}{3} \sin\theta_r V_q + V_o$$

$$V_b = \frac{2}{3} \sin\theta_r V_d + \frac{2}{3} \cos\theta_r V_q + V_o$$

$$V_c = \frac{2}{3} \cos\theta_r V_d - \frac{2}{3} \sin\theta_r V_q + V_o$$

Eq15



Equivalent circuit of PMSM without damper windings.

Equivalent circuit of PMSM

Equivalent circuit is essential for the proper simulation and designing of the motor. It is achieved and derived from the d-q modelling of the motor using the voltage equations of the stator. From the assumption, rotor d axis flux is represented by a constant current source which is described through the following equation,

$$\lambda_f = L_{dm} i_f \quad \text{Eq16}$$

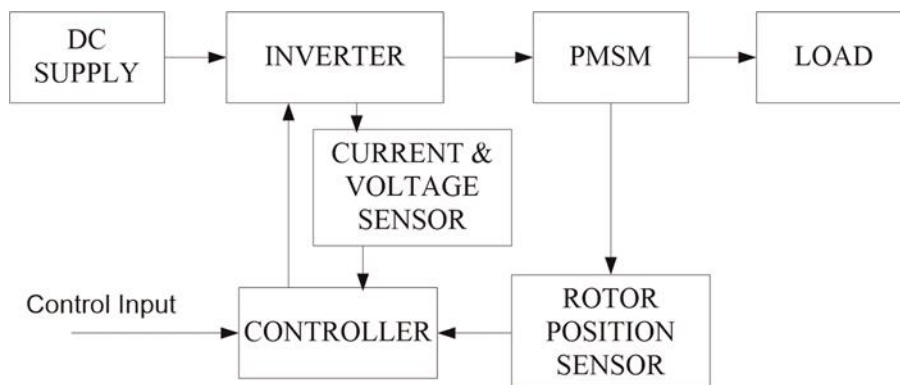
where λ_f , field flux linkage; L_{dm} , d-axis magnetizing inductance; i_f , equivalent permanent magnet field current.

Permanent magnet synchronous motor drive system

The motor drive essentially consists of four main components such as the PMSM, the inverter, the main control unit and the position sensor.

Inverter

For variable frequency and magnitude, voltage source inverters are devices which convert the constant DC voltage level to variable AC voltage. As specified in the function, these inverters are commonly used in adjustable speed drives.



Components permanent magnet synchronous motor drive

Three phase inverters consist of a DC voltage source and six power ON/OFF

switches connected to the PMSM. Selection of the inverter switches must be carefully done based on the necessities of operation, ratings and the application. There are several devices available in the market and these are thyristors, bipolar junction transistors (BJTs), MOS field effect transistors (MOSFETs), insulated gate bipolar transistors (IGBTs) and gate turn off thyristors (GTOs). It has been inferred that MOSFETs and IGBTs are preferred in the industry because of its advantages that the MOS gating permits high power gain and control advantages. MOSFET is considered to be universal power ON/OFF device for low power and low voltage applications, whereas IGBT has wide acceptance in the motor drive applications and other application in the low and medium power range. The power devices when used in motor drives applications require an inductive motor current path provided by antiparallel diodes when the switch is turned off.

5. Control techniques of PMSM

Many techniques based on both motor designs and control techniques that have been proposed in literature to diminish the torque ripples in the PMSM.

Classification of the various control techniques.

Scalar control

One way of controlling AC motors for variable speed applications is through the open loop scalar control, which represents the most popular control strategy of squirrel cage AC motors. It is presently used in applications where information about the angular speed need not be known. It is suitable for a wide range of drives as it ensures robustness at the cost of reduced dynamic performance.

Typical applications are pump and fan drives and low-cost drives. The main idea

of this method is the variation of the supply voltage frequency inattentively from the shaft response (position, angular speed). The magnitude of the supply voltage is changed according to the frequency in a constant ratio. The motor is then in the condition where the magnetic flux represents the nominal value and the motor is neither over excited nor under excited. The major advantage of this simple method is running in a sensorless mode because the control algorithm does not need information about the angular speed or actual rotor position. On the contrary, the significant disadvantages are the speed dependence on the external load torque, mainly for PMSM, and the reduced dynamic performances.

Vector control

The vector control of PMSM allows separate closed loop control of both the flux and torque, thereby achieving a similar control structure to that of a separately excited DC machine, as discussed.

Direct torque control (DTC)

The DTC is one of the high performance control strategies for the control of AC machine. In a DTC drive applications, flux linkage and electromagnetic torque are controlled directly and independently by the selection of optimum inverter switching modes of operation. To acquire a faster torque output, low inverter switching frequency and low harmonic losses in the model, the selection is made to restrict the flux linkages and electromagnetic torque errors within the respective flux and torque hysteresis bands. The required optimal switching vectors can be selected by using the optimum switching voltage vector look-up table. This can be obtained by simple physical considerations involving the position of the stator-flux linkage space vector, the available switching vectors,

and the required torque flux linkage.

Field oriented control (FOC) of PMSM

For the control of PM motors, FOC technique is used for synchronous motor to evaluate as a DC motor. The stator windings of the motor are fed by an inverter that generates a variable frequency variable voltage scheme. Instead of controlling the inverter frequency independently, the frequency and phase of the output wave are controlled using a position sensor.

FOC was invented in the beginning of 1970s and it demonstrates that an induction motor or synchronous motor could be controlled like a separately excited DC motor by the orientation of the stator mmf or current vector in relation to the rotor flux to achieve a desired objective. For the motor to behave like a DC motor, the control needs knowledge of the position of the instantaneous rotor flux or rotor position of permanent magnet motor. This needs a resolver or an absolute optical encoder. Knowing the position, the three phase currents can be calculated. Its calculation using the current matrix depends on the control desired. Some control options are constant torque and flux weakening. These options are based in the physical limitation of the motor and the inverter. The limit is established by the rated speed of the motor, at which speed the constant torque operation finishes and the flux weakening starts. From the literature it has been found that the best control for PMSM to make it to behave like a DC motor using decoupling control is known as vector control or field oriented control. The torque components of flux and currents in the motor are separated by the vector control through its stator excitation.

Steady state torque versus speed.

From the dynamic model of the PMSM, the vector control is derived.

Assuming the line currents as input signals,

$$i_a = I_m \sin(\omega_r t + \alpha) \quad \text{Eq17}$$

$$i_b = I_m \sin(\omega_r t + \alpha - 2\pi/3) \quad \text{Eq18}$$

$$i_c = I_m \sin(\omega_r t + \alpha + 2\pi/3) \quad \text{Eq19}$$

Writing the above Eq. (17) to Eq. (19) in the matrix form,

$$\begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix} = \begin{bmatrix} \cos(\omega_r t + \alpha) \\ \cos(\omega_r t + \alpha - 2\pi/3) \\ \cos(\omega_r t + \alpha + 2\pi/3) \end{bmatrix} I_m \quad \text{Eq20}$$

where α is the angle between the rotor field and stator current phasor, ω_r is the electrical rotor speed.

Using the Park's transformation, the currents obtained in the previous cycle are transformed to the rotor reference frame axis with the rotor speed ω_r . Since α is fixed for a given load torque, the q and d axis currents are fixed in the rotor reference frames. These constant values are made similar to the armature and field currents in the separately excited DC machine. The q axis current is distinctly equivalent to the armature current of the DC machine. The d axis current is field current, but not in its entirety. It is only a partial field current; the other part is contributed by the equivalent current source representing the permanent magnet field. Thus, the q axis current is known as the torque producing component and the d axis current is called the flux producing component of the stator currents.

Substituting Eq. (20) in Eq. (14) and obtaining i_d and i_q in terms of I_m as follows,

$$i_d = I_m \sin\alpha \cos\alpha \quad \text{Eq21}$$

Using Eq. (3), Eq. (4), Eq. (10) and Eq. (21) the electromagnetic torque equation is obtained as given below,

$$T_e = \frac{3}{2} P \frac{2}{\pi} \lambda_m \left[L_d - L_q \right] i_d i_q \sin 2\alpha + \lambda_f i_m \sin \alpha \quad \text{Eq 22}$$

Where L_d and L_q are the d and q axis synchronous inductances. Each of the two terms in the equation has a useful physical interpretation. The first “magnet” torque term is independent of i_d but is directly proportional to the stator current component i_q . In contrast, the second reluctance torque term is proportional to the i_d and i_q current component product and to the difference of the inductance values.

As Eq. (22) shows that the torque depends on the rotor type and its inductances L_d , L_q and on permanent magnets mounted on the rotor. The non-salient PMSM have surface mounted magnets on the rotor and the reluctance term disappears since L_q equals L_d . On the contrary, the electromagnetic torque is more dominated

by the reluctance component when permanent magnets are interior mounted and the rotor’s saliency causes a difference in L_q and L_d .