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Elect/Elect

①  $L = 2\text{m}$   
Velocity flow at smaller end  $= V_1 = 5\text{m/s}$   
Velocity flow at larger end  $= V_2 = 2\text{m/s}$   
Pressure head at smaller end  $= P_s = 2.5\text{m of liquid}$   
Loss of Head  $= \frac{0.35(V_1 - V_2)^2}{2g}$

$$= \frac{0.35(5 - 2)^2}{2 \times 9.81} = 0.161\text{m}$$

Pressure head at larger end  $= P_L$

Bernoulli's eqn

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + Z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + Z_2 + H$$

$$P_s = \frac{P_1}{\rho g} \quad P_L = \frac{P_2}{\rho g}$$

$$Z_1 = 2; Z_2 = 0$$

$$2.5 + \frac{5^2}{2 \times 9.81} + 2 = \frac{P_L}{\rho g} + \frac{2^2}{2 \times 9.81} + 0 + 0.161$$

$$P_L = 5.409\text{m of fluid}$$

② Inlet Diameter =  $D_1 = 20\text{cm}$   
 Throat Diameter =  $D_2 = 10\text{cm}$   
 Inlet Area =  $A_1 = \pi D_1^2 = 314.16\text{cm}^2$

Throat Area =  $A_2 = \frac{\pi D_2^2}{4} = 78.54\text{cm}^2$

Density of water  $\rho = 1000\text{kg/m}^3$

Pressure at inlet =  $17.658\text{N/cm}^2 = 17.658 \times 10^4\text{N/m}^2$

Pressure at inlet =  $\frac{P_1}{\rho g} = \frac{17.658 \times 10^4}{1000 \times 9.81} = 18\text{m}$

$\frac{P_2}{\rho g} = -30\text{cm of Hg}$  S.G. = 13.6

$\frac{P_2}{\rho g} = -30 \times 10^{-2}\text{m of Hg} \times 13.6$   
 $= -4.08\text{m}$

Differential Head =  $\frac{P_1 - P_2}{\rho g}$   
 $= 18 - (-4.08)$   
 $= 22.08\text{m} = 2208\text{cm}$

Using  $Q = \frac{C_d \sqrt{2gh} \cdot A_1 A_2}{\sqrt{A_1^2 - A_2^2}}$

$= \frac{0.98 \times \sqrt{2 \times 9.81 \times 2208} \times 314.16 \times 78.54}{\sqrt{314.16^2 - 78.54^2}}$

$= 165455.3\text{cm}^3/\text{s}$   
 $= 165.455\text{L/s}$

③ Diameter of Pipe = 30 cm  
 $A_1 = \frac{\pi d_1^2}{4} = 706.86 \text{ cm}^2$

Diameter of Orifice = 15 cm  
 $A_2 = \frac{\pi d_2^2}{4} = 176.72 \text{ cm}^2$

Specific gravity of oil = 0.9

Specific gravity of Hg = 13.6

Differential manometer reading  $X = 50$  cm of Mercury  
 $C_d = 0.64$

Differential Head,  $h = X \left( \frac{\rho_m}{\rho} - 1 \right)$

$= 50 \left( \frac{13.6}{0.9} - 1 \right)$

$h = 705.56$  cm of oil

$Q = \frac{C_d \sqrt{2gh} \cdot A_1 A_2}{\sqrt{A_1^2 - A_2^2}}$

$= \frac{0.64 \times \sqrt{2 \times 9.81 \times 705.56} \times 706.86 \times 176.72}{\sqrt{(706.86)^2 - (176.72)^2}}$

$Q = 137443.29 \text{ cm}^3/\text{s}$

$Q = \frac{137443.29}{1000} = 137.444 \text{ l/s}$

(4) Diameter of Mercury head  $\times 2 = 170 \text{ mm} = 0.17 \text{ m}$   
 S.G. of Mercury  $\approx 13.6$   
 S.G. of Sea water  $\approx 1.026$   

$$V = \sqrt{2gh} \quad h = 2 \left( \frac{\rho_2}{\rho_1} - 1 \right)$$

$$= 2 \times 0.17 \left( \frac{13.6}{1.026} - 1 \right)$$

$$= 2.0354 \text{ m}$$

$$V = \sqrt{2 \times 9.81 \times 2.0354} = 6.395 \text{ m/s}$$

$$= \frac{6.395 \times 8600}{1000} = 23.01 \text{ m}^3/\text{h}$$

(5)  $Q = 0.05 \text{ m}^3/\text{min} = 50 \text{ dm}^3/\text{min}$   
 $P = 15 \text{ bar} = 15 \times 10^6 \text{ N/m}^2$   
 Speed  $\approx 1700 \text{ rev/min}$

$$I = 150 \text{ mm} \quad ND = 10 \text{ cm}^2/\text{rev}$$

$$\text{Volumetric efficiency} = \frac{\text{Actual flow rate}}{\text{Ideal flow rate}}$$

$$\text{Ideal flow rate} = \text{Nominal flow rate} \times \text{Speed}$$

$$= 10 \text{ cm}^3/\text{rev} \times 1700 \text{ rev/min}$$

$$= 17000 \text{ cm}^3/\text{min}$$

$$\text{Ideal flow rate} = \frac{17000}{1000000} = 0.017 \text{ m}^3/\text{min}$$

$$\text{Actual flow rate} = 0.05 \text{ m}^3/\text{min}$$

$$\text{Volumetric efficiency} = \frac{0.05}{0.017} = 2.94\%$$

$$\begin{aligned} \text{Fluid power} &= P \times Q \\ &= 15 \times 10^5 \text{ N/m}^2 \times \frac{0.105}{60} \text{ m/s} \end{aligned}$$

$$= 1249.5 \text{ W}$$

$$\text{Shaft power} = \frac{2\pi NP}{60} = \frac{2\pi \times 1700 \times 15}{60}$$

$$= 2670.35 \text{ W}$$

$$\text{Overall efficiency} = \frac{\text{Fluid power}}{\text{Shaft power}}$$

$$= \frac{1249.5}{2670.35} = 0.468 = 46.8\%$$