

NAME: HDIFE NZUBECHUKWU KINGSLY

MATRIC NUMBER: 15/ENG051014

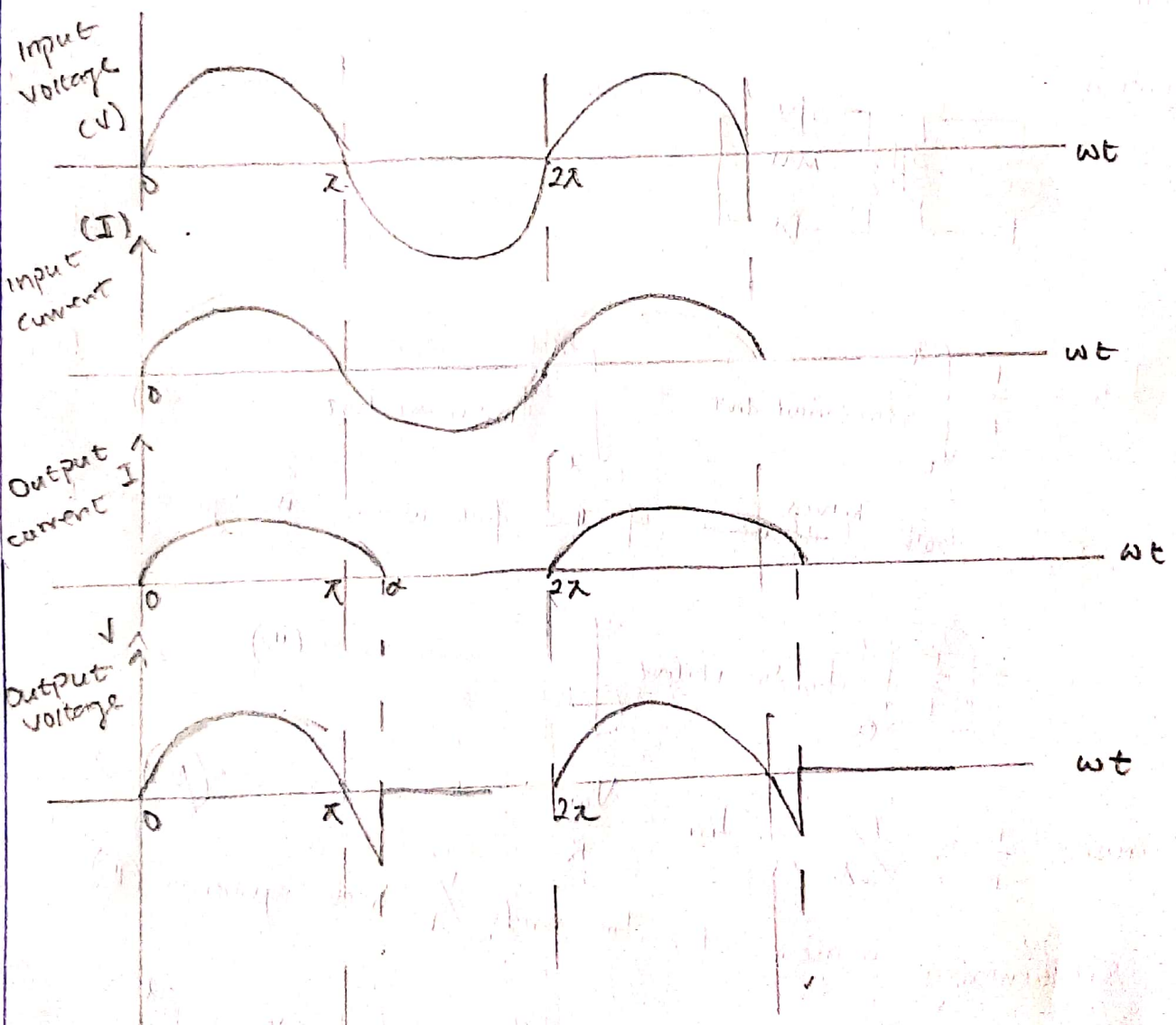
DEPARTMENT: MECHATRONICS ENGINEERING

COURSE: MCT 510

ASSIGNMENT 5

QUESTION 1: (Example 3)

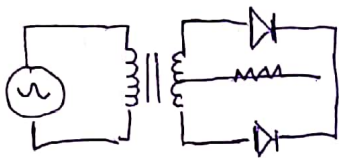
A single phase half wave diode rectifier is feeding an R-L load. Draw the wave shape of the output voltage and current.



### QUESTION 2:

A full wave diode rectifier with centre tapped transformer is feeding a resistive load of  $R$ . Assume the diode has a zero forward resistance and infinite reverse resistance. find the expressions for  $V_{dc}$ ,  $I_{dc}$ ,  $I_{rms}$ ,  $P_{dc}$ ,  $P_{ac}$ , Efficiency ( $\eta$ ), form factor (ff), Ripple factor (RF), TUF, PIV and crest factor (CF). Draw the wave shapes of input voltage & current, output voltage & current. Take  $V_m = 100V$ ,  $R = 5\Omega$

Solution:



$$(1) I_{dc} = \frac{1}{T} \int_0^{\pi} I_m \sin \omega t \, d\omega t + \int_{\pi}^{2\pi} I_m \sin \omega t \, d\omega t \quad \text{--- (I)}$$

Since both <sup>halves</sup> half wave of the full wave is symmetrical

$$2 \left[ \frac{1}{T} \int_0^{\pi} I_m \sin \omega t \, d\omega t \right] \quad \text{--- (II)}$$

where  $\frac{1}{T} = \frac{1}{2\pi}$ ,  $I_m = \frac{V_m}{R}$  :  $\text{--- (B)}$

Substituting values of  $I_m$  and  $\frac{1}{T}$  into equation (II)

$$2 \left[ \frac{1}{2\pi} \int_0^{\pi} \left( \frac{V_m}{R} \right) \sin \omega t \, d\omega t \right] = 2 \left[ \frac{1}{2\pi} \left( \frac{V_m}{R} \right) \int_0^{\pi} \sin \omega t \, d\omega t \right]$$

$$\Rightarrow \left( \frac{2}{2\pi} \right) \left( \frac{100}{5} \right) \int_0^{\pi} \sin \omega t \, d\omega t \quad \text{--- (III)}$$

Integrating equation (iii)

$$\frac{1}{\lambda} (20) \left[ -\cos \omega t \right]_0^{\lambda}$$

$$\Rightarrow \frac{20}{\lambda} \left[ (-\cos(180)) - (-\cos(0)) \right]$$

$$\frac{20}{\lambda} [1 + 1] = \frac{40}{\lambda} = 12.7323 \approx 12.73 \text{ A}$$

(ii)  $V_{dc} = I_{dc} \times R = 12.73 \times 5 = 63.65 \text{ V}$

(iii)  $I_{rms}^2 = \frac{1}{T} \int_0^{\lambda} I_m^2 \sin^2 \omega t \, dt + \int_{\lambda}^{2\lambda} I_m^2 \sin^2 \omega t \, dt \quad \text{--- (i)}$

Since both halves of the full wave are symmetrical

$$2 \left[ \frac{1}{T} \int_0^{\lambda} I_m^2 \sin^2 \omega t \, dt \right] \quad \text{--- (ii)}$$

$\Rightarrow \frac{2}{2\lambda} \int_0^{\lambda} \left( \frac{V_m}{R} \right)^2 \sin^2 \omega t \, dt$    
 Substituting values of  $I_m$  and  $\frac{1}{T}$  from equation (i) into equation (ii)

$$\frac{2}{2\lambda} \left( \frac{100}{5} \right)^2 \int_0^{\lambda} \sin^2 \omega t \, dt \quad \text{--- (iii)}$$

but from trigonometry

$$\sin^2 \theta = \frac{1 - \cos 2\theta}{2}$$

Similarly

$$\sin^2 \omega t = \frac{1 - \cos 2\omega t}{2} \quad \text{--- (iv)}$$

Substituting equation (8) into equation (iii)

(4)

$$\left(\frac{2}{2\lambda}\right)\left(\frac{100}{5}\right)^2 \int_0^{\lambda} \frac{1 - \cos 2\omega t}{2} d\omega t \quad \text{--- (v)}$$

Simplifying equation (iv)

$$\left(\frac{2}{2\lambda}\right)\left(\frac{100}{5}\right)^2 \left(\frac{1}{2}\right) \int_0^{\lambda} 1 - \cos 2\omega t d\omega t$$

$$\left(\frac{2}{4\lambda}\right)\left(\frac{100}{5}\right)^2 \left[ \int_0^{\lambda} \omega t d\omega t - \int_0^{\lambda} \cos 2\omega t d\omega t \right]$$

$$\left(\frac{2}{4\lambda}\right)\left(\frac{100}{5}\right)^2 \left[ \left[ \omega t^2 \right]_0^{\lambda} - \left[ \frac{\sin 2\omega t}{2} \right]_0^{\lambda} \right]$$

$$\left(\frac{2}{4\lambda}\right)\left(\frac{100}{5}\right)^2 \left[ \lambda - \left[ \frac{\sin 2 \times 180}{2} - \frac{\sin 2(0)}{2} \right] \right]$$

$$\left(\frac{2}{4\lambda}\right)\left(\frac{100}{5}\right)^2 [\lambda] = \left(\frac{1}{2\lambda}\right)(400)(\lambda) = 200 \text{ A}$$

$$I_{rms}^2 = 200$$

$$I_{rms} = \sqrt{200} = 14.142 \text{ A}$$

$$(iv) \quad V_{rms} = I_{rms} \times R = 14.142 \times 5 = 70.71 \text{ V}$$

$$(v) \quad P_{dc} = I_{dc}^2 \times R = (12.93)^2 \times 5 = 810.2645 \text{ W}$$

$$\underline{\underline{810.26 \text{ W}}}$$

(5)

$$(vi) P_{ac} = I_{rms}^2 \times R = (14.142)^2 \times 5 = 999.9808$$

$$\approx 999.98 \text{ W}$$

$$(vii) \text{Efficiency} = \frac{P_{dc}}{P_{ac}} = \frac{810.52}{999.98} = 0.8105 \approx 81.05\%$$

$$(viii) PIV = V_m = 100 \text{ V}$$

$$(ix) T_u F = \frac{\frac{V_m}{\pi} \times \frac{V_m}{\pi R}}{\frac{V_m}{2\sqrt{2}} \times \frac{V_m}{2R}} = \frac{\frac{V_m^2}{\pi^2 R}}{\frac{V_m^2}{2\sqrt{2} R}}$$

$$\Rightarrow \frac{V_m^2}{\pi^2 R} \times \frac{2\sqrt{2} R}{V_m^2} = \frac{2\sqrt{2}}{\pi^2} = 0.2865$$

$$(x) \text{Crest factor} = \frac{I_{\text{peak}}}{I_s} = \frac{I_m}{I_{rms}} = \frac{200}{141.42} = 1.4142$$

$$\frac{I_m}{V_m} = 2 //$$

(3) Advantages and disadvantages of

- (i) full wave rectifier using centre tap transformer
- (ii) full wave rectifier using bridge circuit.

### Full wave rectifier using centre tap transformer

#### Advantages

- (i) The output and efficiency of centre tap full wave rectifier are high because AC supply delivers power during both halves
- (ii) For the same secondary voltage bridge rectifier has double output

#### Disadvantages

- (i) Where a small voltage is required to be rectified, the full wave rectifier circuit is not suitable
- (ii) In centre tap transformer, the middle of the secondary winding for tapping is difficult

### Full wave rectifier using bridge circuit

#### Advantages

- (i) It eliminates the use of centre tap transformer.
- (ii) The output is double to that of the centre tapped full wave rectifier for the same secondary voltage
- (iii) The peak inverse voltage across each diode is one-half of the centre tap circuit of the diode

#### Disadvantages

- (i) It needs four diodes
- (ii) The circuit is not suitable when a small voltage is required to be rectified. It is because in this case, the two <sup>diodes</sup> ~~resistors~~ are ~~connected~~ connected in series and offer double voltage drop due to their internal resistance.